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Subsidy Project of Decommissioning and Contaminated Water Management Development of Technology for Investigation inside Reactor Pressure Vessel (RPV)

Interim Report for FY2020

August 2021

International Research Institute for Nuclear Decommissioning (IRID)

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1. Research Background and Purpose

[Purpose of the investigation inside the Reactor Pressure Vessel (RPV)]

To obtain basic information regarding the inside of the RPV (fuel debris distribution, dose, condition of structures, etc.) for fuel debris retrieval.

[Implementation details until FY2019]

The method of accessing the reactor core from the top by opening a hole (hereinafter "top access investigation method") and the method of accessing the reactor core from the side (hereinafter "side access investigation method") were studied. In the previous project "Development of Technology for Investigation inside RPV" (FY2018-19), functional verification of both the methods was carried out through elemental tests of the equipment directed towards actual application, the concept of the method of investigation was examined and the equipment specifications were developed.

> Bottom access investigation method

[Reflections of this project]

Development of Technology for Investigation inside RPV



Information regarding the inside of RPV (Visual information, dose rate, etc.)

Study of fuel debris retrieval method and equipment design



No. 2

Side access investigation method

1. Research Background and Purpose

[Implementation details in this project]

A cutting method using abrasive water jet (AWJ) was developed, as a top access investigation method wherein an opening is created in the reactor internal structures (steam dryer, steam separator, shroud head, etc.) for establishing the access route to the inside of the shroud, while giving priority to reliably cutting the reactor internal structures regardless of their highly uncertain status. However, developing a method for further reducing the secondary waste (abrasive, etc.) resulting from the access route establishment, and a method for controlling the dispersion of radioactive dust during work, has become a challenge. Moreover, with the change in the method of removing spent fuel from Unit 2, engineering work to check how the side access investigation method is actually applicable on site has become a challenge.

Hence, in order to enhance the actual applicability of the top access investigation method, machining technology wherein the secondary waste (abrasive, etc.) generated or the radioactive dust dispersion resulting from cutting, etc. performed inside the RPV is less than that resulting from the conventional abrasive water jet (AWJ), will be developed in this project as a method for creating openings in the reactor internal structures (steam dryer, steam separator, shroud head, etc.) in order to establish the access route to the inside of the shroud.

 \Rightarrow (1) Advancement of machining technology for the top access investigation method

Moreover, since it is anticipated that it would take a certain amount of time until the top access investigation method and the side access investigation method are applied on site, it is important to develop a method that could be used for investigating inside RPV early on, and hence the work of establishing the access route to the inside of PCV is being carried out for the detailed investigation inside PCV.

Therefore, a conceptual study will be conducted in this project, on the bottom access and investigation equipment for investigating inside RPV by inserting the investigation equipment into the RPV from the opening assumed to be present at the RPV bottom by introducing the investigation equipment inside the pedestal using the access route to the inside of the pedestal that has already been established for detailed investigation inside PCV or for increasing the scale of retrieval in stages.

 \Rightarrow (2) Development of the bottom access investigation method



2. Project Goals

Aiming for the TRL of the hole drilling investigation method developed until FY2019

(1) Advancement of machining technology for the top access investigation method

⇒ Feasibility of machining technology involving less secondary waste generated from cutting by means of the conventional abrasive water jet shall be verified as a machining method for establishing the access route to the inside of the shroud for top access investigation.

4

Basic Design

specifications

Elemental test







TRL

7

5

4

pertaining to the bottom access investigation method shall be developed, and engineering shall be carried out based on the results of developing elemental technologies that the method constitutes. Moreover, a conceptual study of the equipment for accessing the inside of RPV and the equipment for investigating inside RPV shall be carried out using the method of accessing the inside of pedestal developed as part of "Development of Technology for Detailed Investigation inside PCV" and several methods in







3. Implementation Items, their Correlations, and Relations with Other Research No. 5





4. Schedule



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5. Project Organizational Chart

The technology for investigation inside RPV has been developed under this project, but for that the interface between each development team becomes important. Hence, by getting involved in development through mutual technological cooperation, domestic plant equipment manufacturers who are organization members of IRID have undertaken a series of tasks including analyzing site conditions, conforming with the fuel debris retrieval plan, etc. to develop technology for safe, proper, reasonable, speedy and site oriented fuel debris retrieval at the Fukushima Nuclear Power Station (1F) and thus IRID Headquarters, Toshiba ESS and Hitachi GE are jointly carrying out development.

International Research Institu (H	d technology management as progress of technology development	Tokyo Electric Power Company Holdings, Inc.Various coordination for the site applicability
 Toshiba Energy Systems & Solutions Corporation (2) Development of the bottom access investigation method ① Development of the bottom access / investigation plan and the development plan for the access / investigation equipment ② Conceptual study of the bottom access / investigation equipment 	 Hitachi-GE Nuclear Energy, Ltd (1) Advancement of machining technology for the top investigation method ① Investigation and evaluation of alternative mach technologies ② Development planning for alternative machining ③ Elemental test and feasibility verification of alter machining technologies (2) Development of the bottom access investigation ① Development of the bottom access / investigation development plan for the access / investigation ② Conceptual study of the bottom access / investigation 	d. Project teams to cooperate for technological development p access Development of Technology for Increasing the Scale of Fuel Debris Retrieval in Stages g technologies trative Development of Technology for Detailed Investigation inside PCV
	Sugino Machine Limited • (1) Structural design concerning advancement of machining techni access investigation method Hitachi Plant Construction, Lto • (1) Investigation of technology of advancement of machining techni access investigation method	g the bology for the top d. concerning the bology for the top

(1) Advancement of machining technology for the top access investigation method

<Purpose>

To develop machining technology wherein the secondary waste (abrasive, etc.) generated or the radioactive dust dispersion is less than that resulting from the conventional abrasive water jet (AWJ) cutting technology, as a method for creating openings in the reactor internal structures (steam dryer, steam separator, shroud head, etc.) to establish the access route to the inside of the shroud.

<Implementation details>

- •The following items were implemented this year targeting the steam separator.
- ① Investigation / evaluation and selection of machining technologies as an alternative to the conventional AWJ technology (implemented for equipment besides the steam separator as well)
- 2 Optimization of the machining parameters with respect to AWJ cutting (reducing the volume of abrasive), and study on AWJ nozzle
- ③ Study on equipment and tools required when the selected machining technologies are applied
- (4) Implementation of simple tests and evaluation of the selected machining technologies, and narrowing down the machining technologies
- (5) Study on the implementation policy for FY2021

<Results>

- ① Alternative machining technologies were investigated and evaluated, and machining technology in which hole saw cutting, circular saw cutting and laser cutting are added to the AWJ cutting technology was selected.
- 2 Equipment required for the above-mentioned 4 methods were studied and it was found that equipment that can be inserted through narrow spaces would be feasible.
- ③ A study was conducted on downsizing the nozzle used in AWJ cutting, the machining parameters were optimized and as a result of conducting simple tests, it was found that it would be possible to substantially reduce the volume of abrasive compared to what was used in the past (8 ton → 0.33 ton).

④ With regards to other machining technologies besides AWJ, laser cutting could be applicable for cutting in the vertical direction.

<Remaining issues>

- ① The applicability of the results of simple tests conducted this year to equipment other than the steam separator, and further reduction in the volume of abrasive.
- (2) Using laser for horizontal cutting



① Investigation and evaluation of alternative machining technologies

The machining technologies were evaluated for each target (steam dryer bottom plate, steam separator, shroud head) as per the following table. The technologies were narrowed down and the AWJ (including WJ) with hole saw, circular saw and laser was selected for the steam separator.

	÷	Processing technology classification	Cutting / grind	ding									Melting							
	targe	Processing	A	В	С	D	E	F	G	Н	- 1	J	K	K'	L	М	Ν	0	Р	Q
No.	Processing	Evaluation item	AWJ cutting (including WJ cutting)	Drill cutting	Cutting by hole saw / core boring / ultrasonic core drill / trepanning	Cutting by circular / saw / circular cutter / circular grinder	Cutting by wire saw	Cutting by band saw	Cutting by saber saw (reciprocating saw)	Cutting by hydraulic cutter	Cutting by chisel	Cutting by milling cutter / end mill	Laser cutti	Laser gougi	Plasma arc cutting	Arc saw cutting	Contact type arc discharge	Consumabl e WJ cutting	Gas cutting	Electrical Discharge Machining (EDM)
1		Material to be cut	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	х	0
2		Thickness of plate to be cut	0	0	0	0	0	0	0	0		0	0		0				-	
3		Surface to be cut (cylindrical)	0	х	Δ	0	0	0	0	0	\bigtriangleup	x							-	
4		Two fold pipe cutting (batch cutting / multi-stage cutting)	0	х	0	0	0	0	0	0		x							-	
5		Cutting speed	0	0	0	0	0	0	0	0	0	0	0						-	
6		Re-processing risk	0	0	0	0	0	0	0	0	\bigtriangleup	0	Δ	Δ	\bigtriangleup				-	
7	rator	Positioning standoff	0	0	0	0	0	0	0	0	0	0	Δ		х	х	х	х	-	
8	m sepai	Angle of the tool with the surface being processed	0	Δ	Δ		Δ	\bigtriangleup	Δ	\bigtriangleup	\bigtriangleup								-	
9	Stea	Work before processing	0	0	0	0	0	0	0	0	0	0							-	
10		Discharge into the reactor core	Δ	Δ	Δ		Δ	\bigtriangleup	\bigtriangleup	\bigtriangleup	\bigtriangleup			Δ	Δ	\bigtriangleup	\bigtriangleup	\triangle	-	
11		Dust dispersion																	-	
12		Processing reaction force	Δ																-	
13		Tool size (incidental equipment)					х	х	х	х	x								-	
14		Device service life (maintainability)																	-	
15		Environmental conditions inside the reactor	0	\bigtriangleup	Δ		Δ	\bigtriangleup	\bigtriangleup		\bigtriangleup	\triangle							-	х
Compre the stea	hensi am se	ve evaluation (Applicability to parator opening)	0	x			х	х	×	х	х	x		- *1	x	х	х	х	-	x
	[Remarks] [Legend]O: Expected to be applicable \triangle : Measures required \square : Cannot be evaluated (trial manufacturing and taste test are required for evaluation) X: Application expected to be difficult -: Application not possible (not evaluated) *1: Since laser gouging is a chipping technology, it was not evaluated. (Laser cutting is a cutting technology that follows the same principle.)								nce laser											



2 Selection of machining technology (multiple options may be selected)

Machining technology was selected as per the study flow indicated in the table below.





(1) Advancement of machining technology for the top access investigation method (*1) Legend for the "Level of priority of the studies"

② Study on optimization of machining parameters / abrasive collection method with respect to AWJ cutting

Factor analysis was conducted for reducing the volume of abrasive discharge, abrasive reduction effect resulting from improving the parameters and the feasibility were studied, and the future response policy was set.

Item / evaluation

Itom / ovoluc	tion					
item / evalua	auon	Major	Medium	Minor		
	High	High	High	Medium		
Feasibility	Medium	High	Medium	Low		
	Low	Medium	Low	Low		

No		Study items		Primary evaluation	Effect	Feasibi	Priority of the studies	Future implementat
	Major	Medium	Minor			lity	(*1)	ion details
1		Not using abrasive (Cutting by means of WJ)	-	Cutting by means of WJ is possible. Cutting performance needs to be verified.	Major	Low	Medium	Simple test
2		Reducing the volume of		Evaluation needs to be conducted by performing cutting tests with the volume of abrasive used per unit of time and the cutting speed as the parameters.	Medium	High	High	Simple test
3		abrasive used per unit of time	-	If an abrasive material (carbide, ceramic, etc.) that has a high cutting performance is used, the nozzle gets worn out faster.	Minor	Medium	Low	-
4	discharge volume	abrasive me		Equipment specifications (nozzle size, nozzle length, etc.) for achieving high cutting performance need to be studied and evaluated.	Medium	Low	Low	Desk study
5	Discharge volume = Volume of abrasive used per unit of time	Reducing the duration of jet spray	Increasing the cutting speed	Since there are prospects that the tool can be downsized (refer to slide 12, 13), it is likely that the cutting speed can be increased by shortening the stand-off and improving cutting performance.	Major	High	High	Desk study Simple test
6	x jet spray duration (for stage 1) x No. of cutting stages	Jet spray duration = Length to be cut / cutting speed	Shortening the length to be cut (Revision of cutting procedures)	Since there are prospects that the tool can be downsized (refer to slide 12, 13), it is likely that the length to be cut can be shortened by revising the cutting procedures.	Major	High	High	Desk study Simple test
7		Reducing the no. of cutting stages	Increasing the cutting depth (Revision of cutting procedures)	Since there are prospects that the tool can be downsized (refer to slide 12, 13), it is likely that the cutting depth can be increased by revising the cutting procedures.	Major	High	High	Desk study Simple test
8		Height of steam separator opening / Cutting depth	Reducing the height of steam separator opening	Cannot be changed.	-	None	-	-
9	Abrasive collection	Collecting while cutting	_	Even through abrasive can be collected using a catcher, etc. after cutting through the cutting target, the range of applicability is small and abrasive reduction effect is limited.	Minor	Low	Low	Desk study
10		Collecting after cutting	-	The volume of abrasive accumulated on top of the shroud head is small due to the high pressure water sprayed during cutting and the abrasive reduction effect is limited.	Minor	Low	Low	Desk study



The dimensional conditions are as follows:

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6. Implementation Details

(1) Advancement of machining technology for the top access investigation method

2-2. Study of the AWJ/WJ nozzle (1/2)

Downsizing of the AWJ/WJ nozzle was studied with the steam separators as the cutting target, which accounted for most of the volume of abrasive used in the FY2019 plan.

Steam

(1) Advancement of machining technology for the top access investigation method

2-2. Study of the AWJ/WJ nozzle (2/2)

AWJ/WJ head were studied, and it was found that AWJ/WJ jet spray would be possible at φ 70 mm or less and in the horizontal direction.

- ⇒ It is expected that the volume of abrasive used can be reduced from the following perspectives, by using a small nozzle that can be inserted into the narrow space in the middle of the 3 casings of the steam separators.
 - Shortening the length to be cut by revising the cutting procedures. \Rightarrow Shortening the cutting duration (reduction in volume of abrasive used)
 - Enhancing the cutting efficiency by closing in on the stand-off. ⇒ Increasing the cutting speed and shortening the cutting duration (reduction in volume of abrasive used)



(*1) Result of preliminary calculations assuming that depth of 50 mm is cut at a time.



2-3. Study on equipment and tools required when each machining technology is applied

Of the various machining technologies, tool heads for hole saw cutting, circular saw cutting and laser cutting were studied from the perspective of whether or not the cutting tool head fits in the cutting equipment (outer diameter ϕ 140 mm or less) developed until FY2019.

Simple tests or desk study were conducted for each technology as there were prospects that the outer diameter of each cutting tool head would be ϕ 140 mm or less.



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2-4. Study on propriety of cutting with a stand-alone technology and on combining cutting technologies (1/5)

The propriety and the strong points/weak points of each machining technology that is expected to be feasible in each cutting direction (vertical / horizontal) was evaluated and the propriety of applying a stand-alone cutting technology or a combination of technologies was studied.

4

Hole saw

AWJ/WJ

(1) Technology expected to be feasible as a stand-alone technology \Rightarrow AWJ/WJ and circular saw (*1)

3

Circular saw

AWJ/WJ

(2) Technologies expected to be feasible in combination \Rightarrow AWJ/WJ, circular saw, laser, hole saw

[Combination of machining technologies]

Vertical

direction

Horizontal

direction

1

AWJ/WJ

AWJ/WJ

No.

Combination

of technologies

[Conceptual image of cutting the steam separator (middle section)]

2

Laser

AWJ/WJ

Cutting in the vertical direction

Cutting in the horizontal direction

Circular saw Circular saw Circular saw

7

Circular saw

Removing the cut piece





Stage 1 cutting completed



5

AWJ/WJ

Circular saw

6

Laser

No. 15



8

Hole saw





(2)-4. Study on propriety of cutting with a stand-alone technology and on combining cutting technologies (2/5) Cutting procedure for the steam separators, which accounted for most of the volume of abrasive used in the FY2019 plan, was studied.

[AWJ/WJ] An example of Combination No. 1 of machining technologies is shown in the

figure below (refer to Slide 15 for the Combination No.)

(1) Advancement of machining technology for the top access investigation method

(2)-4. Study on propriety of cutting with a stand-alone technology and on combining cutting technologies (3/5) Cutting procedure for the steam separators, which accounted for most of the volume of abrasive used in the FY2019 plan, was studied.

[Laser] An example of Combination No. 2 of machining technologies is shown in the figure below (refer to Slide 15 for the Combination No.)



Vertical cutting

No. 17

Vertical cutting

(Only middle

(1) Advancement of machining technology for the top access investigation method

(2)-4. Study on propriety of cutting with a stand-alone technology and on combining cutting technologies (4/5) Cutting procedure for the steam separators, which accounted for most of the volume of abrasive used in the FY2019 plan, was studied.

[Circular saw] An example of Combination No. 7 of machining technologies is shown in the figure below (refer to Slide 15 for the Combination No.)



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(1) Advancement of machining technology for the top access investigation method

(2)-4. Study on propriety of cutting with a stand-alone technology and on combining cutting technologies (5/5) Cutting procedure for the steam separators, which accounted for most of the volume of abrasive used in the FY2019 plan, was studied.

No. 19

[Hole saw] An example of Combination No. 4 of machining technologies is shown in the figure below (refer to Slide 15 for the Combination No.)



ID

2-5. Evaluation of the impact on other systems

Factors having an impact on other systems were studied and evaluated for each cutting technology.

	Items		AWJ	Circular saw	Hole saw	Laser			
	Ma	achining dust	Minor	Major	Major	Minor			
Influencing factor	Pro	cessing water	Present	Present	Present	Absent			
inititiencing factor	Abrasive / air		Present	Absent	Absent	Present			
	Sys	tem heat input	Minor	Minor	Minor	Minor			
		Impact	Units 1 / 3: Medium to major and Unit 2: Medium	Mi	Units 1 / 3: Medium to major and Unit 2: Medium				
	bust emissi	Volume of dust dispersion •Rise in PCV pressure	Major	Mir	Minor				
	on control	Evaluation	 The objects to be cut should be sarequired, and a qualitative study o Cutting should be performed in sta (penetration part, etc.) from the RF be seguentially reflected in the cut 	ampled for contamination density, and the f the preliminary estimations and actual ages based on the work achievements of V into PCV should be carried out in pa ting plan.	jet should be investigated as ispersion should be conducted. onitoring at the site of leakage as monitoring and the results should				
	 Unit 1: Medium, Unit 2: Minor to major, Unit 3: Minor to medium Study bearing in mind the criticality risk due to falling of fuel debris from inside RPV. Relative comparison between the volume (est debris remaining inside RPV in each Unit 								
Impact on other systems	ality control	Evaluation	 Fuel debris that did not fall even a is unlikely to fall due to comparativ structures, falling of cut pieces, etc It is desirable to conduct prior inversity. 	Fuel debris that did not fall even after the application of external forces such as aftershocks after the earthquake disaster, cooling water injection, etc is unlikely to fall due to comparatively small external pressure such as that of machining water being used while machining the reactor internal structures, falling of cut pieces, etc. (However, concrete evaluation is difficult) It is desirable to conduct prior investigation of places where machining equipment or machining byproducts are likely to fall and check for criticality risks.					
	<	Impact	Medium		Minor				
	Vaste disposal	Evaluation	 Objects being cut and machining of Hence work of adding collection and certain percentage or less (needs As for equipment specifications, ter respectively. It has been confirmed during the in facility. 	Objects being cut and machining dust (garnet is added in case of AWJ) increase the volume of waste. Hence work of adding collection and storage equipment as well as the cost increases. However, the impact is limited since the waste generated is certain percentage or less (needs to be verified in the future) of the quantity assumed during retrieval. As for equipment specifications, technology for collecting waste that is inside PCV and for waste that flows into the system is being developed respectively. It has been confirmed during the investigation inside PCV that elution of garnet does not have any impact on the operation of the water treatment					
	Fuel debris retrieval		The secondary waste released at the time of fuel debris retrieval is being evaluated, but it is estimated that the amount will be larger than the amount generated from machining of reactor internal structures obtained as a result of investigation inside RPV.						
Evaluation of cutting technology (Propriety of application)			 Currently, although there are some unknowns with regards to the impact of the 4 machining methods mentioned in this table on other systems, the impact is expected to be minor or limited. Currently none of the methods seem to have any crucial impact, but elemental tests will be conducted and the methods will continue to be studied. 						



(1) Advancement of machining technology for the top access investigation method

2-6. Planning for simple tests with revised parameters and abrasive collection method

The following tests are planned to be conducted with the purpose of studying how the volume of abrasive used for the AWJ cutting (including WJ cutting) can be reduced and the method of collecting the abrasive.

Implementation items	Simple test items	Target machining technology	Items to be verified	
[Evaluation of AWJ/WJ technology] Study on reducing the volume of abrasive used when the AWJ technology is used, and abrasive collection method.	Cutting conditions verification test	AWJ/WJ	 Cutting performance in the vertical direction Cutting performance in the horizontal direction 	Implemented in test No. 23 and 24
	Dust dispersion verification test	AWJ/WJ	Discharge into the reactor	(*1)
	Nozzle life verification test	AWJ/WJ	Nozzle life	(*2)
	Abrasive collection test	AWJ	Volume of abrasive collected	(*3)

- (*1) Availability of implementing the dust dispersion verification test with the narrowed down machining technologies as the subject, and the test plan are planned to be studied based on the simple tests conducted this year.
- (*2) The nozzle life verification test is planned to be conduced with the narrowed down machining technologies as the subject based on the simple tests conducted this year.
- (*3) Simple tests will not be conducted since the volume of abrasive used is expected to substantially reduce based on the result of the cutting conditions verification test indicated in Slide 23 and 24, and since the volume of abrasive collected is expected to be limited based on the results of the desk study on abrasive collection.



(1) Advancement of machining technology for the top access investigation method

2 -7. Planning for simple tests on the feasibility of the studied machining technologies

The following tests will be conducted for AWJ cutting (including WJ cutting), hole saw cutting, circular saw cutting and laser cutting, for which simple tests are necessary, to verify cutting performance.

	Implementation items	Simple test items	Target machining technology	Items to be verified	
(*1) Material generated as a result of machining, which is likely to fall inside the reactor, on top or on the		Multi-fold pipe cutting	AWJ / WJ / Hole saw / circular saw / laser	Cutting performance in the vertical direction	Test results are indicated in Slide
	[Simple tests on the machining Re technologies] tes Comparison of AWJ with other Se machining (*1) technologies		AWJ / WJ / Circular saw	Cutting performance in the horizontal direction	Propriety of implementing the tests with the
		Required positioning accuracy verification test	AWJ / WJ / Hole saw / circular saw / laser	Position accuracy during cutting (Range of fluctuation)	narrowed down machining technologies as the subject, and the test plan are planned to be studied based on the simple tests.
side of the shroud head. (However, this shall not		Reaction force verification test	AWJ / WJ / Hole saw / circular saw / laser	Reaction force during cutting	Test results are indicated in Slide No. 24 to 28.
 Include cut pieces. For example, abrasive from the AWJ or dross from laser cutting, etc.) (*2) For example, the necessity to remove the dross from the machining performed the previous time. 		Secondary waste volume (*1) verification test	AWJ / WJ / Hole saw / circular saw / laser	 Risk of re-machining the discharge into the reactor Re-machining risk 	in Slide No. 29. Propriety of implementing the tests with the
		Dust dispersion verification test	Hole saw / circular saw / laser	Discharge into the reactor	harrowed down machining technologies as the subject, and the test plan are planned to be studied based on the simple tests.
		Pre-machining (incidental) work ^(*2) verification test	AWJ / WJ / Hole saw / circular saw / laser	Cutting performance on machined surface	Verification of the requirement of pre- machining (incidental) work during the "Multi-fold pipe cutting verification test"
		Equipment life (maintainability) verification	AWJ / WJ / Hole saw / circular saw / laser	·Life of the tool	Propriety of implementing the tests with the narrowed down machining technologies as the subject, and the test plan are planned to be studied based on the simple tests.

[Scope (red frame) of verification by means of the multi-fold pipe cutting verification test]

No		1	2	3	4	5	6	7	8
Combining technologies	Vertical direction	AWJ/WJ	Laser	Circular saw	Hole saw	AWJ/WJ	Laser	Circular saw	Hole saw
	Horizontal direction	AWJ/WJ	AWJ/WJ	AWJ/WJ	AWJ/WJ	Circular saw	Circular saw	Circular saw	Circular saw



(1) Advancement of machining technology for the top access investigation method

2-8. Implementation and evaluation of simple tests (AWJ/WJ: Cutting conditions verification test)

[Overview]

- (1) A flat plate test piece (plate thickness 3 mm (*1)) was cut to confirm availability of cutting and appropriate cutting speed.
 - (*1) The plate thickness (3.2 mm) of the outer casing part of the steam separator was simulated.
- (2) A simulated double pipe was cut according to the cutting procedures indicated in Slide No. 16, to confirm the availability of cutting in the vertical and horizontal directions as well as appropriate cutting speed.

[Results (flat plate cutting / WJ)]

 The flat plate test piece could not be cut by WJ in the shortest stand-off condition (stand-off: 1 mm) of the cutting procedures, therefore a cutting test for the simulated double pipe was not conducted.

[Results (flat plate cutting / AWJ)]

- ① The flat plate test piece could be cut by AWJ at 600mm/min, the highest speed of the test equipment.
 - Stand-off: 20mm
 - Volume of abrasive supplied: 500g/min



Results of flat plate test piece cutting test (AWJ / Stand-off: 20mm)

(1) Advancement of machining technology for the top access investigation method

2-8. Implementation and evaluation of simple tests (AWJ/WJ: Cutting conditions verification test)

[Results (Double pipe cutting / AWJ)]
① The double pipe test piece could be cut by AWJ following the planned cutting procedures.
[Cutting speed] Vertical cutting (only outer casing): 30mm/min
Vertical cutting (outer casing + middle casing): 110mm/min
Horizontal cutting: 40°/min

- (2) In case of cutting at the above-mentioned speed, the total amount of abrasive used for cutting the main body of the steam separator is tentatively calculated to be approx. 0.33 ton (approx. 8 ton last year).
- ③ AWJ cutting reaction force was applied approximately 40N in the direction opposite to the AWJ jet spray, therefore measures need to be taken in the future.



Conceptual image of cutting the steam separator

A result of partially simulated steam separator cutting test (AWJ)



(1) Advancement of machining technology for the top access investigation method

2-8. Implementation and evaluation of simple tests (Laser: Multi-fold pipe cutting verification test)

[Overview]

- (1) Laser cutting specifications \Rightarrow Laser type: Fiber laser / Assist gas: Air
- (2) A simulated double pipe was cut in the vertical direction according to the cutting procedures indicated in Slide No. 17, to confirm the availability of cutting and appropriate cutting speed.

[Results]

- ① Although dross was found at the distal end where laser cutting is terminated, since it does not get re-deposited, the simulated double pipe could be cut.
- ② Cutting in the vertical direction is expected to be possible (speed at which cutting can be performed: up to 600 mm/min). A reaction force of 8N was formed in the direction opposite to the assist gas jet, but as the laser head was inclined vertically downwards at approx. 12.5°, the reaction force applied in the horizontal direction is expected to be approx. 1.7N which is smaller than that in the case of AWJ.



Results of partially simulated steam separator cutting test (Laser)

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(1) Advancement of machining technology for the top access investigation method

2-8. Implementation and evaluation of simple tests (circular saw: Multi-fold pipe cutting verification test) (1/2)

[Overview]

(1) A simulated double pipe and a simulated three fold pipe were simultaneously cut as per the cutting procedures indicated in Slide No. 18, and the cutting propriety in the vertical direction as well as the speed at which cutting can be performed were verified.

[Results (cutting in the vertical direction)]

- ① The double pipe and three fold pipe could be cut simultaneously, however the cutting was unstable as there arose fluctuations in the rotational speed during cutting.
- ② In addition, since the cutting speed was extremely low at 0.5 mm/min, the result showed that application of vertical cutting direction for the steam separator may not be realistic.
- ③ Inadequate rotating torque due to the design for downsizing the tool, or increase in cut resistance as the blade simultaneously comes in contact with 5 locations can be considered to be the causes for unstable cutting. (*1)



Photo of cut portion of a simulated double pipe



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(1) Advancement of machining technology for the top access investigation method

2-8. Implementation and evaluation of simple tests (circular saw: multi-fold pipe cutting verification test) (2/2)

[Overview]

(1) A simulated double pipe was cut in the horizontal direction to verify availability of simultaneously cutting two double pipes in the horizontal direction in accordance with the cutting procedures indicated in slide No. 18.

[Results (cutting in the horizontal direction)]

When cutting two steam separators simultaneously, the circular saw feed needs to accomplish up/down cut simultaneously in one cutting.

First of all, the down cut and up cut were cut individually at a time in this test. The result of the test showed that the down cut was not successful and so simultaneous cutting of two steam separators was not possible.





(1) Advancement of machining technology for the top access investigation method

2-8. Implementation and evaluation of simple tests (hole saw: Multi-fold pipe cutting verification test) [Overview]

(1) Two simulated double pipes were simultaneously cut in accordance with the cutting procedures indicated in slide No. 19, and availability of cutting in the vertical direction as well as the speed at which cutting can be performed were verified.

[Result]

- ① The amount of hole saw feeding in the vertical direction was approximately 1 mm and it suspended due to overload (cutting speed: 0.5mm/min).
- (2) Increasing the rotational torque of the hole saw can be considered for improving cutting performance, but with the current tool configuration and restrictions on dimensions, major increase in torque seems unlikely and hence hole saw is not applicable.



2-8 Implementation and evaluation of simple tests (final evaluation)

[Overview]

The preliminary calculations pertaining to the volume of secondary waste and the working time were added to the simple test results (slide No. 23 to 28) and the prospects of actually applying each machining technology were evaluated. Further, since the result of the flat plate cutting test showed that WJ cutting is not possible, it was not included in the evaluation.

[Result]

The circular saw and hole saw are not applicable in the actual site whereas AWJ and laser have prospects of actual application.

Mac	Machining technology		/J	Laser	Circul	Hole saw	
nems		Vertical	Horizontal	Vertical	Vertical	Horizontal	Vertical
Cutting availability		Good	Good	Good	Acceptable	Unacceptable	Unacceptable
Volume of secondary waste	Evaluation	Good	Good	Good	Good	—	—
	Abrasive (kg)	182.7	141.1 ^(*1)	0.0	0.0	—	—
	Machining dust	7.0	1.2 ^(*1)	2.4	2.7	—	—
	Total (kg)	189.7	142.3(*1)	2.4	2.7	—	—
Working Time	Evaluation	Good	Good	Good	Unaccepta ble	—	—
	Working time (min)	365.4	282.1 ^(*1)	29.7	18900 (315h)	—	—
Evaluation		Good	Good	Good	Unacceptable	unacceptable	Unacceptable

(*1) Volume of secondary waste resulting from AWJ cutting in the horizontal direction and corresponding working time when cutting of the main

body of the steam separator is repeated in the vertical direction at a 50 mm pitch. (*2) Even though cutting was possible, it was unstable due to lack of rotational torque (refer to Slide No. 26).



(1) Advancement of machining technology for the top access investigation method

2-9 FY2021 Implementation Policy

[Narrowing down combinations of machining technologies]

From the evaluation results (slide No. 29) based on the results of simple tests, the 2 patterns of machining technology combinations were narrowed down as shown in the following table.

Combination	Combination of		(*1)	No. 2 (*2)		
machining		Vertical	Horizontal	Vertical	Horizontal	
teenneregiee		AWJ	AWJ	Laser	AWJ	

(*1) Corresponds to the No. in the table on Slide No. 15.

[FY2021 Implementation Policy]

The FY2021 implementation policy on the machining technologies (AWJ & laser) that have been narrowed down are shown below.

Machining technology		Implementation Details
AWJ	1	Study on application to parts other than the main body of steam separator
	2	Study on further reducing the volume of abrasive (revision of cutting parameters)
	3	Elemental tests concerning $\textcircled{1}$ and $\textcircled{2}$ as may be required (Nozzle life will be verified during the elemental tests.)
Laser	1	Study on applications other than the steam separator
	2	Study on application to cutting in the horizontal direction (study on downsizing the head)
	3	Elemental tests concerning $\textcircled{1}$ and $\textcircled{2}$ as may be required
	4	Identification of issues in actual application and study of measures



(2) Development of the bottom access investigation method

Definition of development items: Definition of access equipment and investigation equipment

The technology to be applied to the method of investigating inside RPV from the bottom was divided into the following 3 parts and studied.



(i) Equipment for access to the inside of the pedestal

(ii) Equipment for access to the inside of the RPV from inside the pedestal

(iii) Investigation equipment



(2) Development of the bottom access investigation method

① Planning of the bottom access / investigation and the development for the access / investigation equipment

The study process is shown below.

Implementation items	Unit 1	Unit 2	Unit 3		
1. Drafting of the investigation	n plan				
A. Organization of investigation needs	 ⇒ Verification of investigation needs with TEP Information such as image data and dose rate Existing technological development results with the second second	CO and NDF e needs to be obtained by accessing the inside of th vill be utilized for early implementation.	ne RPV early on.		
B: Organization of preconditions	Preconditions will be organized based on resu	Its of investigation inside PCV, etc.			
C: Organization of applicable technologies	 (i) Equipment for access to the inside of the pedestal ⇒ Access equipment used for Detailed Investigation inside PCV will be used. 	 (i) Equipment for access to the inside of the pedestal ⇒ Arm type access equipment for fuel debris retrieval will be used. 	 (i) Equipment for access to the inside of the pedestal ⇒ Similar to Unit 2, arm type access equipment for fuel debris retrieval will be used , since the plan is to reduce the PCV water level. 		
 ⇒ Equipment that have been developed in preceding projects that are currently in development and preparation, and which can be applied for this purpose will be put together. ⇒ Study conditions will be set based on the results of "B: 	(ii) Equipment for access to the inside of the RPV from inside the pedestal (using a drone) ⇒ Since it has been evaluated that most of the fuel debris has fallen to the pedestal bottom, study will be carried out afresh presuming that there is an opening of diameter about 1m in the central part of the lower hemispherical dome of the RPV.	 (ii) Equipment for access to the inside of the RPV from inside the pedestal (using telescopic mechanism) ⇒ Study will be carried out afresh presuming that there is an opening in the RPV bottom part above the location where the upper tie plate had fallen, and that the dimensions of the opening are such that the tie plate can pass through it. 	 (ii) Equipment for access to the inside of the RPV from inside the pedestal (using telescopic mechanism) ⇒ Study will be carried out afresh presuming that there is an opening in the RPV bottom part that is about the size of the CRGT based on the investigation result that CRGT had fallen. 		
Organization of preconditions					
	 (iii) Investigation equipment ⇒ Study will be conducted on application of the 	e equipment developed so far including those deve	eloped in other PJs, for each Unit.		
-					



Common for Units 1, 2 and 3





(2) Development of the bottom access investigation method

Unit 1: Development of equipment for accessing the inside of the RPV using a drone

<Purpose>

To perform simple tests on the method of accessing the inside of RPV from inside the pedestal using a drone (wired, wireless), and to evaluate its feasibility as a bottom access investigation method for Unit 1.

<Implementation details>

① A simple flight test of the drone (wired, wireless) was performed for evaluating feasibility.

Drone unit test

•Combination test with extension rod, etc. in an environment with simulated CRD opening / RPV opening (2) Study on response plan for FY2021 based on the simple tests results

<Results>

① Data (size, payload, battery life) contributing to the conceptual study in FY2021 and the essential points of the investigation (ability to pass through the opening, investigation procedures) were verified through simple tests.

② It was determined that the following structure of the drone (wired, wireless) is applicable.

- Wired drone: The structure consisting of a drone and a cable drum was selected.
- Wireless drone: The structure consisting of a drone and an extension rod was selected.

<Remaining issues>

- ① Wired drone: Stable supply of feeding voltage, lack of flight level due to voltage drop in the power supply cable.
- (2) Wireless drone: Extended flight duration
- ③ Common: Evaluation of the site applicability (radiation resistance, darkness and rainfall environment)







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(2) Development of the bottom access investigation method

1. Drafting the investigation plan D: Study of feasibility evaluation items

<Investigation Overview>

- (6) Auxiliary equipment (installed in front of the CRD opening part)
 - 1) Cable drum (only for wired drone)
 - Feeding and retraction of the wired drone cable is carried out with the cable drum.
 - 2) Extension rod (utilizing the technology being developed as part of Investigation inside PCV)
 - In the case of wired drone: The cable feed mechanism is installed at the tip of the extension rod, it is ensured that the wired drone cable does not get entangled in the cables of existing equipment inside the pedestal and the load on the drone resulting from the cable mass is reduced.
 - In the case of wireless drone: The operation transmitter / image receiver are installed at the tip of the extension rod to communicate with the wireless drone inside the pedestal.



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No. 37

Unit

6. Implementation Details(2) Development of the bottom access investigation method

1. Drafting the investigation plan D: Study of feasibility evaluation items

<Access route up to the pedestal (CRD opening part)>

In the demonstration test concerning the investigation inside Unit 1 PCV, the PCV is accessed from the guide pipe of the X-2 penetration and from there the CRD opening part is accessed by moving anti-clockwise inside PCV.



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(2) Development of the bottom access investigation method

1. Drafting the investigation plan D: Study of feasibility evaluation items

<Investigation pattern using drones (wired and wireless)>

No.	Pattern 1 Wired drone and extension rod	Pattern 2 Only wired drone	Pattern 3 Wireless drone and extension rod	Pattern 4 Only wireless drone
Investigation equipment	Wired drone	Wired drone	Wireless drone	Wireless drone
Auxiliary equipment	 Cable feed mechanism Extension rod Cable drum 	① Cable drum	 Extension rod Transceiver 	① Transceiver
Outline of investigation	 Auxiliary equipment (①②③) are installed in front of the CRD opening part. The extension rod extends inside the pedestal before or after the drone flies. The inside of the RPV is investigated by means of the flying drone. 	 Auxiliary equipment (①) is installed in front of the CRD opening part. The inside of the RPV is investigated by means of the flying drone. 	 Auxiliary equipment (①②) are installed in front of the CRD opening part. The extension rod extends inside the pedestal during or after the drone flies. The inside of the RPV is investigated by means of the flying drone. 	 Auxiliary equipment (①) is installed in front of the CRD opening part. The inside of the RPV is investigated by means of the flying drone.
Conceptual diagram	Drone Cable			
Cable drum	Extension rod Cable feeding mechanism	Cable drum E	Extension rod Transceiver	Transceiver



Unit 1

	tems	Conditions	
	Location for access inside the PCV	 Guide pipe for inserting the equipment for investigation inside PCV being established in the X-2 penetration Guide pipe inner diameter: φ314mm (usable space: φ290mm) 	[Maximum permissible size] Φ290mm (*1)
Dimensional	Location for access inside of the pedestal	 CRD opening part Dimensions of the opening part: width 790mm × thickness 1200mm × height 1173mm (from the top of the grating) 	(*1) The size of the opening at the bottom part of RPV is assumed to be φ 1000mm, however, due to access route constraints the maximum permissible size is φ .
Conditions	Outer diameter of the opening at the bottom of the RPV • φ1000mm • It is assumed that there is a cylindrical space of φ1000mm below the RPV opening.		290mm. In future, the position control performance, etc. of the access equipment will be evaluated and the
	Location of the RPV bottom opening	Center of the RPV	regions that can be investigated will be studied.
	Dose rate	Dose rate: 100 Gy/hr (tentative), Cumulative dose: 1000Gy	
	Temperature	Assumed to be 80°C or less	
Environmental Conditions	Humidity	Assumed to be 100%	
	Other	 Darkness Cooling water injection in progress (rainfall) Since it is assumed that there is damage caused on the grating inside the pedestal due to the impact of falling of fuel debris, as far as possible the equipment should not come in contact. 	
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(2) Development of the bottom access investigation method

1. Drafting the investigation plan D: Study of feasibility evaluation items

<Required specifications and preconditions for the actual investigation>

Required specifications:

- (1): Should be able to reach the top surface of CRD housing (height 7m).
- (2): Should be able to verify the inside of the RPV bottom in the range of tilt: $\pm 90^{\circ}$, pan: $\pm 180^{\circ}$ by operating the drone or the mounted camera.

-Droconditiones



Unit

(2) Development of the bottom access investigation method

1. Drafting the investigation plan D: Study of feasibility evaluation items

<Overview of the investigation equipment and auxiliary equipment (specifications and functions)>

		Mounted equipment / specifications and functions					
Equipme	ent name	Pattern 1	Pattern 2	Pattern 3	Pattern 4		
Investigation equipment	Drone	 Type : Wired drone Size : within φ290mm Flight level: 7m Investigation equipment: (1) Camera (2) Dosimeter (3) Motor for oscillating the camera 		 Type : Wireless drone Size : within φ290mm Flight level: 7m Investigation equipment: (1) Camera (2) Conceptual image transit (3) Dosimeter (3) Dosimeter (4) Transmitter for dosime (5) Motor for oscillating the second second	a nsmitter for camera eter ne camera		
	Cable Drum	 Feeding and winding the drone cab Length of cable that can be stored: 	le approx. 15m	_			
Auxiliary	Cable feed mechanism	 Feeding the drone cable Motor driven 	_	_			
equipment	Extension rod	Introducing the cable feed mechanism into the pedestal Extension length approx. 5.3m Air driven		Introducing the wireless transceiver into the pedestal Extension length approx. 5.3m Air driven			
	Transceiver	Wired (operation /	image)	Wireless (operation: 2.4Ghz,	image: 5.7GHz)		



No. 42

Unit





Unit 1



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- (2) Development of the bottom access investigation method
- 1. Drafting the investigation plan D: Study of feasibility evaluation items



Unit 1

6. Implementation Details (2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc. [Wired drone]

<Development issues concerning wired drones, response policy (target specifications) and simple test details>

Unit

Classification	Development issues	Response policy (target specifications)	Simple test	Items to be verified	Test No.	Study results
	Size	Shall be structured so that it can pass through the inner diameter of guide pipe (φ290mm)	Single unit test	Size	1-1	Refer to No. 47
Main hady of	Payload	The combined weight of the drone main body and the cable shall be such that it can be hauled.		Payload, flight level	1-1	Refer to No. 47
wired drone	Flight stability	Shall be able to fly through a 1000mm diameter opening and shall be controlled only with the help of the image from the mounted camera.	Combined test	Ability to pass through CRD / RPV opening	1-5 1-6	Refer to No. 51 and 52
	View area (Scope of investigation)	 Shall be able to fly up to the top surface of CRD housing (height 7m) Shall be able to view 90° vertically and 360° horizontally 	Single unit test	Ability to rotate	1-2	Refer to No. 48
	Stable power supply	Power supply of 350V shall be possible at 50m				Only specifications
Cable	Stable communication	Shall be able to be controlled even at the farthermost location. And, images shall be uninterrupted.	-	-	-	were studied (detailed study planned to be conducted in FY2021)
	Propriety of cable feeding / winding	Assuming that the drone flies up to the interior of the RPV, 15m of cable shall be able to be fed / wound remotely	Single unit	Propriety of cable feeding /	1-3	Refer to No. 49
	Size	Size shall be smaller than a semi-circle of $\phi 290 \text{mm}$ as it is mounted on to the crawler.	1001	in the second seco		
Cable Drum	Structure	Shall be able to be operated remotely. Shall be motor-driven.	-	-	-	Detailed study planned to be conducted in FY2021
	Torque	Assuming that the drone flies up to the interior of the RPV, the torque shall be able to haul a 15m cable. (Trial evaluation needs to be conducted)	-	_	_	Detailed study planned to be conducted in FY2021
Cable feed	Propriety of cable feeding / winding	Shall be mounted at the tip of the extension rod and shall be able to feed / wind 7m of cable remotely in order to make the drone fly up to the RPV interior.		Propriety of cable feeding / retracting	1-4	Refer to 50.
meenamsm	Structure	The basic structure shall have a passive pulley.				
	Structure	Multistage CFRP (*1) rods shall be drawn out by means of air drive.				Taskaslas
Extension rod	Size	Size shall be smaller than a semi-circle of $\phi 290\text{mm}$ when not extended, as it is mounted on to the crawler.		-		developed as part of other subsidized projects is used.
	Payload	Cable feed mechanism shall be able to be mounted at the tip.				
	(*1) (*1) C	ERP: Carbon Fiber Reinforced Plastics		Cinternational Research Instit	ute for Nucle	ear Decommissioning

(2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc. [Wired drone] Test No.: 1-1

<Unit test: Wired drone (size, payload, flight level)>

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[Overview] (1) The size of the wired drone was verified.

(2) The payload of the wired drone was verified.

•A simulated cable for measuring the flight level was installed on the drone, the drone was flown up to a height to which the cable could be raised, the length of the cable that could be hauled was measured, and the payload was calculated based on the unit weight of the cable.

- [Result] (1) The size of the drone was length 438mm, width 270mm and height 47.4mm, and it could pass through the inner diameter of the guide pipe which was less than φ290mm.
 - (2) The flight level was about 3 to 5 m, and the payload calculated from the length of cable hauled was 465 to 800g. Due to a voltage drop in the power supply cable, the target flight level of 7m could not be reached. Hence the specifications of the power supply cable need to be revised.



(*1) A wireless drone was simulated with the specifications of a wired drone and the test was conducted.



No. 48

Unit 1

6. Implementation Details (2) Development of the bottom access investigation method 2. Feasibility study E: Performing tests, etc. [Wired drone] Test No.: 1-2

<Unit test: Wired drone (ability to turn)>

[Overview] (1) Since the panning function of the camera is supposed to work for the turning movement of the drone, the deviation from the guiding center was verified to confirm turning performance.

[Result] (1) The drone turned φ 2 to φ 2.5m at a flight level of 1 to 2m, and φ 1 to φ 1.5m at a flight level of 4 to 5m, which is larger than the size of the RPV opening, which is φ 1. Hence it would not be able to turn within φ 1m.

- (2) In order to enhance the turning performance of the drone, it is necessary to change the current arrangement of the 4 propellers from their current rectangular placement to a more square shaped placement so that the propellers become equidistant, however, this is difficult to achieve due to dimensional constraints. (If the propellers are arranged at long equal intervals along the length of the drone, the inner diameter of the guide pipe becomes φ290mm or more and hence this arrangement is not possible. And, if the propellers are arranged at short equal intervals along the width of the drone, the space available for mounting equipment such as flight controller, etc. is reduced and the required equipment cannot be mounted.)
- (3) Due to the above-mentioned factors, measures to enhance turning performance will not implemented, and the method of not making the drone turn inside the RPV opening as far as possible will be applied but investigating the status inside the RPV bottom, which was going to be verified by turning the drone, from a height in the vicinity of the top surface of the CRD housing, by installing a camera with a pan-tilt mechanism on the under surface of the drone, will be studied.



Test conditions (flight level: 1 to 2m)



Visually estimating the deviation from the guidance center of the simulated RPV opening part

No. 49

Drone

Unit

Simulated RPV opening part guidance center

Test conditions (flight level: 4 to 5m)



(2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc. [Wired drone] Test No.: 1-3

<Unit test: Cable drum (propriety of cable feeding / winding)>

[Overview] (1) Availability of cable feeding and winding was verified when a 15m long cable is stored in the cable drum (manual).

[Result] (1) The outer diameter of the composite cable for the wired drone was studied, and a manual cable drum was test manufactured.
 (2) Availability of cable feeding and winding was verified and a 15m long cable can be stored in a size of φ290mm.





Unit

(2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc. [Wired drone] Test No.: 1-4

<Unit test: Cable feed mechanism (propriety of cable feeding / retracting operation)>

[Overview] (1) Availability of cable feed/pullback operation with cable feed mechanism was verified [Result] (1) It was verified that cable feed mechanism can feed a cable in 7m length required for the drone and pullback a cable.





Unit 1

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(2) Development of the bottom access investigation method

6. Implementation Details

2. Feasibility study E: Performing tests, etc. [Wired drone] Test No.: 1-5

<Combination test with the extension rod, etc.: Ability to pass through the CRD / RPV opening part, whether or not the cable gets entangled, investigation / movement pattern>

[Overview] (1) The wired drone, cable feed mechanism, extension rod and cable drum were combined and the movement was verified by simulating the CRD opening part and the RPV opening part.

(2) The movement was confirmed for the following 2 patterns as per the movement procedures during investigation.

- •Movement pattern A: Onward path Return path Return path Flying the drone to right below the RPV opening part (hovering on stand-by) \rightarrow drawing out the extension rod \rightarrow moving Lowering the drone to right below the RPV opening part (hovering on stand-by) \rightarrow drawing in the extension rod \rightarrow flying the drone outside the CRD opening part
- Movement pattern B: Onward path Drawing out the extension rod \rightarrow flying the drone to right below the RPV opening part \rightarrow moving the drone upwards / investigating

Return path Flying the drone outside the CRD opening part \rightarrow drawing in the extension rod

[Result] (1) Movement pattern A is suitable considering the risk of the drone cable getting caught in the extension rod.

[Evaluation legend] O: No problem, Δ : There is concern, \times : Not possible

No.	Ability to pass through CRD opening part	Ability to pass through RPV opening part	Cable getting caught	Conceptual image from the camera while flying	Remarks
Movement pattern A	0	0	0	0	 The cable came in contact with the floor while the drone was being lowered from the RPV opening part.
Movement pattern B	0	0	Δ	0	 The cable came in contact with the floor while the drone was being lowered from the RPV opening part. On the return path, there was an event of the cable being caught in the extension rod.



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[Flying state] RPV opening [Camera image] Test condition (while passing through the RPV opening part)







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opening part. [Result] (1) The drone flight may be possible inside the pedestal and RPV even if not using the cable feed mechanism and the extension rod for

preventing the cable from getting caught in the CRD opening part, etc., which is designed to reduce the load resulting from cable mass. However, it is necessary to consider measures to prevent the contact of the floor (by synchronizing the drone flight and cable drum winding operation) as the cable contacts with the floor while the drone is being lowered.

[Evaluation legend] O: No problem, \triangle : There is concern, \times : Not possible

No.	Ability to pass through CRD opening part	Ability to pass through RPV opening part	Cable stuck	from the camera while flying	Remarks
1	0	0	0	0	The cable came in contact with the floor while the drone was being lowered from the RPV opening part.

Test condition (while moving upwards to the RPV opening part)

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(2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc. [Wired drone] Test No.: 1-6

< Combination test with the extension rod, etc.: Ability to pass through the CRD / RPV opening part, whether or not the cable stuck, investigation / movement pattern>

[Overview] (1) The wired drone and cable drum were combined and the movement was verified by simulating the CRD opening part and the RPV

Flying direction of the drone (downwards) Flying direction of the drone (upwards) **RPV** opening Drone **RPV** opening Drone part part

> CRD opening part

> > Cable



Test condition (while moving downwards from RPV opening part)







(2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc. [Wireless drone]

<Development issues concerning wireless drones, response policy (target specifications) and simple test details>

Classification	Development issues	nent Response policy (target specifications)		Items to be verified	Test No.	Study results
	Size	Shall be structured so that it can pass through the inner diameter of guide pipe (φ 290mm)	Single unit test	Size	2-1	Refer to No. 54
	Payload	The weight of the drone main body can be hauled	Single unit test	Payload, flight level	2-1	Refer to No. 54
Main body of wireless drone	Battery life	Flight ability for 10 minutes (tentative) (Assuming that the investigation time is 1 min - 4 minutes and the time for flying a round trip is 6 minutes)	Single unit test	Flight duration	2-2	Refer to No. 55
	Flight stability	Flight ability in a range of 1000mm diameter and shall be controlled only with the help of the image from the mounted camera.	Combined test	Ability to pass through CRD / RPV opening, etc.	2-5	Refer to No. 58
	View area (Scope of investigation)	 Flight ability up to the top surface of CRD housing (height 7m) Visual confirmation of 90° vertically and 360° horizontally 	Single unit test	Ability to rotate	2-3	Refer to No. 56
Wireless system	Communication stability	Communication ability in environments through the entire or part of the PCV concrete, control rod drive mechanism and lower head of RPV, even if the signal strength reduces.	Single unit test	Verification of communication performance	2-4	Refer to No. 57
	Structure	Multistage CFRP (*1) rods shall be extended with the air drive.				Technology
Extension rod	Size	Size shall be smaller than a semi-circle of φ 290mm when stored, as it is mounted on to the crawler.	-	-	_	developed as part of other subsidized
	Payload	Transceiver can be mounted at the tip.				projects is used.

(*1) CFRP: Carbon Fiber Reinforced Plastics



No. 54

Unit 1

(2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc. [Wireless drone] Test No.: 2-1

<Unit test: Wireless drone (size, payload, flight level)>

[Overview] (1) The size of the wireless drone was verified.

(2) The payload of the wireless drone was verified.

• A simulated cable for measuring the flight level was installed on the drone, the drone was flown up to a height to which the cable could be raised, the length of the cable that could be hauled was measured, and the payload was calculated based on the unit weight of the cable.

- The upper limit of the payload was verified by adding weight to the lower part of the wireless drone and making it fly.
- [Result] (1) The drone with the size of 438mm length, 270mm width and 47.4mm height passed through the inner diameter of the guide pipe which was less than φ290mm.
 - (2) The flight level was approximately 9 ~ 10m, and the payload calculated from the length of cable traction was 882g on an average.
 - (3) When a weight of 900g, 1000g, 1100g and 1200g was added to the drone, there was no problem until the weight added was 1100g. When 1200g of weight was mounted on the drone, upward flight was possible but wobbling of the drone increased and as the current value of the propeller motor exceeded 80A as against the battery current (3.5A), due to which the battery could get damaged, the upper limit of payload for this drone was considered to be 1100g.



Unit

(2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc. [Wireless drone] Test No.: 2-2

<Unit test: Wireless drone Continuous flight duration (battery life))> [Overview] (1) Continuous flight duration of the wireless drone (battery life) was verified.

[Result] (1) Following are the results of verifying the continuous flight duration (battery life) of the wireless drone.

- Hovering: 4min 23s to 4min 40s
- Repeating upward and downward movement: (round trip between 1 to 7m) 2min 26s to 2min 36s, (round trip between 1 to 2m) 2min 35s to 3min 22s
- (2) If the investigation time inside RPV is 10min (tentative) (assuming that the investigation time is 1 4 minutes and the time for flying a round trip is 6 minutes), since there is no margin in the flight duration, measures such as increasing the size of the battery or installing multiple batteries are needed.



[External appearance of the drone: top surface]



[External appearance of the drone: underside]



[Hovering : Flight level 1 to 2m]



[Repeating upward and downward movement : Round trip of flight level 1 to 2m]



Unit 1



Test condition



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(2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc. [Wireless drone] Test No.: 2-3

<Unit test: Wireless drone (ability to turn)>

- [Overview] (1) Since the panning function of the camera is supposed to work by means of the turning movement of the drone, the deviation from the guiding center was verified to confirm turning performance.
- [Result] (1) The drone turned $\varphi 2m$ at a flight level of 1 ~ 2m, and $\varphi 4$ to $\varphi 7m$ at a flight level of 4 ~ 5m, which is larger than the size of the RPV opening, which is $\varphi 1$. Hence it would not be able to turn within $\varphi 1m$.

(2) In order to enhance the turning performance of the drone, it is necessary to change the current arrangement of the 4 propellers from their current rectangular placement to a more square shaped placement so that the propellers become equidistant, however, this is difficult to achieve due to dimensional constraints. (If the propellers are arranged at long equal intervals along the length of the drone, the inner diameter of the guide pipe becomes φ290mm or more and hence this arrangement is not possible.

And, if the propellers are arranged at short equal intervals along the width of the drone, the space available for mounting equipment such as flight controller, etc. is reduced and the required equipment cannot be mounted)

(3) Due to the above-mentioned factors, measures to enhance turning performance will not implemented, and the method of not making the drone turn inside the RPV opening as far as possible will be applied but investigating the status inside the RPV bottom, which was going to be verified by turning the drone, from a height in the vicinity of the top surface of the CRD housing, by installing a camera with a pan-tilt mechanism on the under surface of the drone, will be studied.



Test conditions (flight level: 1 ~ 2m)



Unit

Visually estimating the deviation from the guidance center of the simulated RPV opening part

No. 57

Simulated RPV opening part auidance center

Test conditions (flight level: 4 ~ 5m)



Unit

(2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc. [Wireless drone] Test No.: 2-4

<Unit test: Wireless drone (verification of ability to communicate)>

- [Overview] (1) The ability to communicate based on the position of the drone and the transceiver was verified. (The drone was placed inside the RPV (plate thickness 200mm) and the transceiver was placed inside the pedestal, and the ability to communicate from an assumed RPV opening of φ1000mm was verified.)
- [Result] (1) A transceiver was placed inside a mock-up facility with radio shielding and the drone was flown through a simulated opening of φ1000mm. The drone was operated at any location regardless of the location of the transceiver and the φ1000mm opening. At this time, the normal signal intensity of -45dBm became about -57dBm due to the radio shielding on the mock-up facility.
 - (2) In order to measure the signal intensity that would result in the drone not being able to fly, the drone was placed inside a metal container with plate thickness 28mm and a radio shielding unit test was conducted. It was confirmed that the signal was attenuated up to about -85dBm, but the drone was still operated. It is presumed that signal leaked through a small gap in the container and thus complete radio shielding was not achieved.
 - (3) The drone was not operated when the transmitter was wrapped in 2 layers of shielding sheet and the drone was placed on a different floor at a distance of approx. 25m to 30m.

However, radio waves other than the drone signal were measured and since these were difficult to be distinguished from the drone signal, the signal intensity was not measured.

- (4) Based on the above, it is presumed that the drone was operated in (1) since radio shielding comparable to the 200mm plate thickness of RPV was not achieved and signal had been leaking.
- (5) In the actual equipment, although the radio waves are completely shielded in the RPV, it is believed that the drone is operable depending on the location of the φ1000mm opening part, and the drone & transceiver. Hence testing methods and conditions in which radio shielding equivalent to the actual RPV can be achieved, need to be studied, tested and verified.



Test image (verification of the attenuation effect in the testing facility)



Test image (verification of the attenuation effect when shielding methods are combined)



6. Implem	ent	ation Deta	ails			Unit 1		No. 59	
(2) Developm	(2) Development of the bottom access investigation method								
2. Feasibility study E : Performing tests, etc. [Wireless drone] Test No.: 2-5									
<combination test="" with<br="">[Overview] (1) The wire part and</combination>	the exte less dro the RP\	ension rod, etc.: Abilit one and extension roc / opening part.	y to pass through the I (with transceiver mo	CRD / RPV opening unted on its tip) were	part, investigation / m combined and the m	novement pattern> ovement was verified by sir	nulating the CR	D opening	
 (2) The movement was verified for the following 2 patterns as per the movement procedures during investigation. Movement pattern A: Onward path Flying the drone to right below the RPV opening part (hovering on stand-by) → drawing out the extension rod → moving the drone upwards / investigating Return path Lowering the drone to right below the RPV opening part (hovering on stand-by) → drawing in the extension rod → flying the drone outside the CRD opening part 									
- Mov	ement p	attern B: Onward path	n Draw	ving out the extension	rod \rightarrow flying the drop wards / investigating	ne to right below the RPV o	pening part $ ightarrow$ n	noving the	
		Return path	n Flying	g the drone outside th	e CRD opening part	\rightarrow drawing in the extension	ı rod		
[Result] (1) Although th suitable sin	ere was ce there	no significant differe was no hovering on s	nce in movement patt stand-by time.	ern A and B, conside	ring the flight duratior [Evaluation legend]	n (battery life), movement particular O : No problem, \triangle : There is	attern B was fou s concern, × : No	und to be ot possible	
No		Ability to pass through CRD opening part	Ability to pass through RPV opening part	Cable getting caught	Conceptual image from the camera while flying	Remarks			
Movement	oattern A	0	0	_	0	During the downward movement opening part, there was an error the drone crashed.	from the RPV in operation and		
Movement	oattern B	0	0	_	0				
Extension rod CRD opening part Drone CRD opening part Drone CRD opening part Drone CRD opening part Drone CRD opening part Drone									



[Flying state]

Test condition (passing through the CRD opening part)







[Flying state]

[Camera image] RPV opening

Test condition (passing through the RPV opening part)



(2) Development of the bottom access investigation method

3. Feasibility evaluation F: Evaluation based on the test results <Evaluation of the simple tests results>

[Evaluation result legend] \circ : Applicable, \triangle : Can become applicable upon revising the specifications, etc., x: Application is difficult, -: Out of scope of evaluation

Unit

Outline of investigation		Pattern 1		Pattern 2		Pattern 3		Pattern 4 (*1)	
Investi	gation equipment		Wired drone	Wired drone			Wireless drone	Wireless drone	
Auxiliary equipment		 Cable feed mechanism Extension rod Cable drum 		① Cable drum		 Extension rod Transceiver 		1 Transceiver	
	Flight level	Δ	Cannot fly to the required height of 7m due to drop in voltage.	Δ	Same as on the left	0	Can fly to the required height of 7m.	0	Same as on the left
	Flight duration (Battery life)	0	Unlimited.	0	Same as on the left	Δ	Limited.	Δ	Same as on the left
Evaluation	Communication stability	_	No wireless communication	_	Same as on the left	Δ	Difficult to completely block the radio waves (same is presumed for actual equipmen as well).	Δ	Same as on the left
items	Ability to pass through CRD opening part	0	Does not come in contact with simulated CRD opening part.	0	Same as on the left	0	Does not come in contact with simulated CRD opening part.	0	Same as on the left
	Ability to pass through RPV opening part	Δ	Sometimes there is contact with the simulated RPV opening part and the flight is not smooth.	Δ	Same as on the left	Δ	Sometimes there is contact with the simulated RPV opening part and the flight is not smooth.	Δ	Same as on the left
	Combination with auxiliary equipment inside the pedestal	Δ	The cable may get caught in the drawn out extension rod.	_	Not applicable	0	No problem in particular.	-	Not applicable
(*4)	/td) The fact we will a fact term A and an active time from the fact we will a fact term O								

(*1) The test results of pattern 4 are an estimation from the test results of pattern 3.

Although flight level is a challenge, the wired drone that does not have a limit on flight duration will be used. (Pattern 2 that does not have the risk of the cable getting caught, and which has fewer equipment configurations, will be used.)

And, the wireless drone will be considered as a back-up for the wired drone. (Pattern 3 will be used assuming there is the risk of radio shielding in the actual equipment.)





No. 61

Unit

- (2) Development of the bottom access investigation method
- 3. Feasibility evaluation F: Evaluation based on the test results

[Proposed Response Policy for FY2021] Based on the results of the simple tests, the issues will be studied in FY2021.

Classification Issues		[Proposed Response for FY2021]
	Stable supply of feeding voltage	 Selecting a DC-DC converter that can drive the motor for the propeller
Wired drone (Pattern 2)	Lack of flight level due to voltage drop in the power supply cable	 Reducing the weight of the power supply cable (with high voltage and low current specifications) Test manufacturing the composite cable (operation system, power supply, camera) Test manufacturing the small high voltage type motor and ESC along with reducing the weight of the power supply cable (it is surmised that the small low voltage type used this time can be used if a DC-DC converter that can convert high voltage to low voltage can be mounted)
Wireless drone (Pattern 3)	Extension of flight duration	 Increasing the battery capacity and the no. of batteries mounted
Common	Radiation resistance	 Irradiation test at the component level and desk study
(Environmental conditions)	Darkness, rainfall	 Considering conducting tests in darkness Selecting equipment in accordance with water-proofing standards



(2) Development of the bottom access investigation method

Unit 2 & 3: Development of equipment for accessing the inside of the RPV using telescopic mechanism

<Purpose>

To perform simple tests on the method of accessing the inside of RPV from inside the pedestal by mounting an access equipment that uses telescopic mechanism, on to the arm type access equipment for fuel debris retrieval, and to evaluate its feasibility as a bottom access investigation method for Unit 2 and 3.

<Implementation details>

The following 3 types of simple tests were implemented.

- O CFRP bonded part strength verification test
- O Sealing performance verification test
- O Behavior verification test

<Results>

The basic performance (stretching movement, extension) of the 14 stage telescopic access equipment, the design of which is being studied, was verified through simple tests using a three-stage telescopic pipe. Issues such as high sliding resistance or leakage from the sealed portion came forth, however, it was evaluated that the mechanism itself was feasible.

<Remaining issues>

- •Reducing the sliding resistance and the amount of leakage from the sealed portion
- Coordinating the specifications and working with arm type access equipment being developed under other projects



No. 62

Unit 2 & 3



IRID

(2) Development of the bottom access investigation method

1. Drafting of the investigation plan C: Organization of applicable technologies

(i) Equipment for access to the inside of the pedestal

Unit 2: Status of development of the technology for increasing the scale of fuel debris retrieval in stages Using the arm-type access equipment being developed under the "Development of Technology for Increasing the Scale of Fuel Debris Retrieval in Stages" project was considered, and a meeting was held for coordinating with said project so as to be able to make the equipment work without making any modifications, etc. as far as possible.

The operation of the tip tool (main working conditions if absolutely no modifications will be made) is described below.

- The tip tool shall be connected to the arm at the tool changer part at the tip of the arm for retrieval.
- As far as dimensional constraints are concerned, the total length of the tip tool inside the enclosure shall be 700mm.
- While removing the contaminated tool from the enclosure, the tool must be placed in a container called DPTE350, but as the depth of the container is approx. 400mm, it should be possible to break up the tool being mounted on the arm so that it fits in the container.
- With regards to dimensional constraints, the diameter of the equipment shall be φ 250mm and the cross-sectional shape of the equipment shall be such that it can pass through X-6 penetration.
- The conveyable weight of the arm shall be 15kg.
- The utilities that can be supplied to the tool at the tip are restricted due to the specifications of the cable installed on the arm.
- The tool at the tip shall be handled by dual armed manipulator (Dexter). And, a hoisting tool needs to be installed. Etc.

The restrictions are rigid. Conditions for relaxing those restrictions will be developed by taking operation related actions or other minor changes.





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6. Implementation Details

- (2) Development of the bottom access investigation method
- 2. Feasibility study D: Study of feasibility evaluation items

Environmental conditions and preconditions pertaining to the bottom access investigation method for Unit 2 and 3

- Dose rate: 100Sv/h
- Temperature: 50° C
- Humidity: 100%
- Other: Darkness, rainfall, fog
- Location for temporarily setting up the RPV bottom opening part
- •Unit 2: In the vicinity of CRD housing 46-39
- •Unit 3: At CRD housing 38-35

- > Outer diameter of the opening at the bottom of the RPV
 - •Unit 2: 187mm (based on the upper tie plate dimensions)
 - •Unit 3: 284mm (based on the external dimensions of the CR guide tube)
- Status of the structures below the location for temporarily setting up the RPV bottom opening part:
 - ·Unit 2: There is a cylindrical space of φ 187mm below RPV bottom opening part
- ·Unit 3: There is a cylindrical space of φ 284mm below RPV bottom opening part









<Rough specifications of the telescopic pipe>

When retracted: approx. 1m When extended: approx. 8m

6. Implementation Details

(2) Development of the bottom access investigation method

- Pipe size : 14 stage configuration from $\phi 97$ to 32mm
- Material: CFRP
- Thickness: 1mm
- Weight: approx. 12kg (with camera and cable drum)



In order to be able to extend up to approx. 8m within the dimensional constraints of φ 100mm and length approx. 1m, a thin walled telescopic pipe with multi-stage configuration needs to be developed.



No. 66

Unit 2 & 3

(2) Development of the bottom access investigation method

Issues pertaining to the bottom access investigation method for Unit 2 and 3 (1/2)

Content in red: Items to be verified through simple tests

Unit 2 & 3

No.	Major items	Medium items	Minor items	Development issues	Response Policy for FY2020	
1	Equipment for access to the inside of the pedestal	Verifying the connection with the arm type access equipment for retrieval	Verifying the detailed specifications of the arm type access equipment for retrieval	 Accuracy in determining the location at the tip Deflection and vibrations of the arm Range of movement of each shaft Conveyable weight Specifications of the cable installed outside the arm Emergency response policy 	 Confirmation with the "Increasing the Scale of Retrieval in Stages" PJ for information that would contribute to the study on equipment specifications 	
2			retileval	Verifying the attachment / detachment method and specifications	 Verification of the feasibility of the transportation container and the procedures for transfer in and out of the enclosure Method of installing and removing using Dexter 	•Confirmation with the "Increasing the Scale of Retrieval in Stages" PJ for information that would contribute to the study on equipment specifications
3			Studying the basic structure	 Viability of the structure given the dimensional constraints associated with handling by means of the arm type access equipment for retrieval 	•Design study Understanding the impact of environmental conditions on the strength of the telescopic pipe at the location where the CFRP rods are attached, along with wall thinning of the pipe, through test manufacturing and demonstration.	
4	Equipment for access to the inside of the RPV from inside the pedestal	Designing the telescopic access equipment	Understanding the behavior while extending/retracting	 Accuracy in connecting the sections (pipe inclination) Vibrations while extending (investigation equipment part) Extent of gap with the tip when the vertically installed mechanism is extended (backlash, deflection) Verification of the extension retraction behavior when the telescopic mechanism is tilted Verification of the extension retraction movement when something gets stuck (Can the telescopic mechanism be extended when it is stuck, can it be retracted when the investigation equipment is stuck) Impact of adhered substances on the extension retraction behavior 	• Design study Understanding the behavior through test manufacturing and demonstration using a multi-stage telescopic mechanism for information that would contribute to the equipment specifications study	
5			Understanding the operating characteristics while extending/retracting	Air pressure required while extending Ability to control position determination Sliding resistance of the air packing and telescopic mechanism Sliding resistance of the rotation control guide of the telescopic mechanism	 Design study Understanding the impact on the sealing performance and sliding resistance under environmental conditions (dose, temperature) assumed as a result of test manufacturing and demonstration, for information that would contribute to the equipment specifications study. Understanding the behavior through test manufacturing and demonstration using a multi-stage telescopic mechanism for information that would contribute to the equipment specifications study. 	
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2. Feasibility study E: Performing tests, etc.



(2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc.

Issues pertaining to the bottom access investigation method for Unit 2 and 3 (2/2)

Content in red: Items to be verified through simple tests

No.	Major items	Medium items	Minor items	Development issues	Response Policy for FY2020	
				·Accuracy in measuring the wire tension (propriety of detecting sagging)		
				•Coordinated control of air pressure and tension while winding the cable when the telescopic mechanism is being extended/retracted	Design study Understanding the behavior through test manufacturing and demonstration	
6	Equipment for		Designing the cable winding mechanism	Limit detection	using a multi-stage telescopic mechanism for information that would	
	access to the inside of the RBV/ from inside	Designing the telescopic access		Placement of the mechanism (passing through X-6 penetration, interference with the arm)	contribute to the equipment specifications study	
	the pedestal	equipment		Pressure resistant box design (about 0.1MPa)		
7			Emergency measures	 Handling of power cutoff (disconnection, etc.), loss of control (software crash), control line disconnection, etc. 	⇒ Will be studied after the overall equipment configuration has been determined.	
8			Designing the slide mechanism	 Placement of the mechanism (passing through X-6 penetration, interference with the arm) 	Design study	
9			Designing the outer form of the investigation equipment	Interference with the X-6 penetration, reactor internal structures	•Design study	
10			Cable design	•Achieving a small diameter (targeting φ6 or less) •Tensile strength	Design study	
11		Investigation equipment designing		Noise countermeasures	 Noise while rotating when the slip ring is used (dosimeter) 	⇒ Will be implemented after the design of the cable winding mechanism shapes up based on the results of the behavior verification test
12	Investigation equipment		Countermeasures for substances adhering to the camera, lighting, etc.	•Design study	⇒ Will be implemented in FY2021 along with the study on the application of a CMOS camera using a cable with a smaller diameter	
13					Visibility	 Verification of the visibility of the back side when there are structures or mechanisms in the vicinity of the camera Understanding the characteristic of reduced visibility due to noise resulting from radiation dose
14			Emergency measures	 Handling of power cutoff (disconnection, etc.), loss of control (software crash), control line disconnection, etc. 	⇒ Will be studied after the overall equipment configuration has been determined.	
15		Operability	Operability using a camera	 Can the operation be performed by determining the status such as status of contact with structures, etc. by means of the camera on the wrist part or the investigation equipment camera 	⇒ Will be studied after the specifications of the arm type access equipment for retrieval are finalized.	
16	Other	Emergency measures	Examination of assumption items	•Which events such as earthquake, power outage, etc. are assumed?	 ⇒ Will be studied after the overall equipment configuration has been determined. ⇒ Will be studied after the specifications of the arm type access equipment for retrieval are finalized. 	



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(2) Development of the bottom access investigation method

2. Feasibility study D: Study of feasibility evaluation items

Telescopic access equipment: Rough specifications



Items	Specifications	Remarks
No. of stages	14 stages	
Material	Pipe: CFRP, aluminum Other parts: aluminum parts	
Driving source	Extension: air Retraction: Cable winding equipment Various motors: power supply	
Pipe thickness	1mm	
Dimensions when retracted (Only telescopic pipe)	1100mm or less	
Dimensions when extended (Only telescopic pipe)	7100mm or more	
Outer diameter	Base: φ97mm Tip: φ37mm	
Air pressure	At maximum extension: 0.1MPa	The plan is to apply air pressure gradually according to the no. of stages
Maximum conveyable weight	2kg (when air pressure is 0.1MPa)	
Cable	Built into the telescopic pipe	
Cable handling	Controlled by the rotation of the reel of the cable winding equipment at the base	
Clearance between the pipes	0.2mm	
Sealant	NBR	Radiation resistance: Cumulative resistance 1 MGy



1013 (when retracted)

Unit 2 & 3 No. 69

- (2) Development of the bottom access investigation method
- 2. Feasibility study D: Study of feasibility evaluation items

Telescopic access equipment: Seal structure

> A seal structure using a wear ring was studied in addition to the seal structure with a track record, in order to control inclination.





Unit 2 & 3

(2) Development of the bottom access investigation method

- 2. Feasibility study E: Performing tests, etc.
- ➤Feasibility evaluation (test)

3 types of tests were conducted on the telescopic access equipment studied as the "(ii) Equipment for access to the inside of the RPV from inside the pedestal".

- (1) Test for verifying the strength of the CFRP bonded part of the telescopic access equipment
- (2) Sealing performance verification test of the telescopic access equipment
- (3) Behavior verification test of the telescopic access equipment

Items to be verified through the tests (Minor items in No. 66 and 67)	Corresponding feasibility evaluation tests
3. Studying the basic structure	(1) Test for verifying the strength of the CFRP bonded part of the telescopic access equipment
4. Understanding the behavior while extending/retracting	(3) Behavior verification test of the telescopic access equipment
5. Understanding the operating characteristics while extending/retracting	(2) Sealing performance verification test of the telescopic access equipment(3) Behavior verification test of the telescopic access equipment
6. Designing the cable winding mechanism	(3) Behavior verification test of the telescopic access equipment



Unit 2 & 3

- (i) Equipment for access to the inside of the pedestal
- ⇒ Arm type access equipment for fuel debris retrieval will be used
- (ii) Equipment for access to the inside of the RPV from inside the pedestal
- ⇒ Will be newly developed (telescopic access equipment)
- (iii) Investigation equipment
- ⇒ Equipment studied under "Development of Technology for Investigation inside RPV" in the previous year will be used.


(2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc. (1) CFRP bonded part strength verification test

<Purpose>

To verify the strength of the location where the CFRP rods are bonded, under assumed environmental conditions.

<Test overview>

Using a sample piece of a small CFRP, shear load was applied to the bonded part, and fracture stress was verified. The radiation environment was simulated by using a CFRP rods bonded part already exposed to radiation as a test piece. Further, the impact of environmental conditions was verified by conducting the test under 0Gy (unirradiated) and 1000Gy (assuming 10 hours under 100Gy/h) exposure conditions.

Furthermore, ISO19095 (resin-Metal bonding characteristics evaluation test method) was used as reference for the test method (Same as the test method for verifying the strength of the CFRP and aluminum bonded part evaluated in the past).

<Evaluation items, etc.>





Unit 2 & 3

No. 72

the

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(2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc. (1) CFRP bonded part strength verification test

<Test results>

O Indoor environment

The shear failure stress after radiation exposure was 21.4 to 26.7 [MPa], that is on an average: 24.2 [MPa], as against 21.0 to 24.0 [MPa], that is on an average: 22.1 [MPa] for the unirradiated sample. Thus there was no major difference in the bonding strength. And, in case of both, the irradiated test piece and the unirradiated test piece, there was a cohesion failure wherein a fracture occurred inside the adhesive layers and hence it is believed that the adhesive did not degrade due to radiation exposure.

O Constant temperature environment with temperature: 50°C and humidity: 95%.

The shear failure stress after radiation exposure was 24.7 to 33.9 [MPa], that is on an average: 28.8 [MPa], as against 23.9 to 29.7 [MPa], that is on an average: 26.8 [MPa] for the unirradiated sample. Thus there was no major difference in the bonding strength. And, in case of both, the irradiated test piece and the unirradiated test piece, there was a cohesion failure wherein a fracture occurred inside the adhesive layers and hence it is believed that the adhesive did not degrade due to radiation exposure. Fracture stress at the CFRP bonded part for 24 hours under



Based on the above results it was evaluated that there is no degradation of the CFRP bonded part due to shear failure stress if it is left for less than 24 hours (*1) under an environment with temperature: 50[°C], humidity: 90%, dose rate: 100[Gy/h] assumed while investigating inside RPV.

(*1) Based on the result that there was cohesion failure, it was evaluated that strength can be retained even when kept under a radiation exposure environment for about 24 hours, just like the results of a similar bonding strength test conducted in FY2019.







(2) Development of the bottom access investigation method 2. Feasibility study E: Performing tests, etc. (2) Sealing performance verification test <Test overview>

The test was conducted with the purpose of verifying sealing performance and sliding resistance of the telescopic access equipment under environmental conditions assumed on the site. The 2 types of structures of the sealed part as shown in the figure on the right were used for the test.

Dose conditions were 0Gy (unirradiated) and 1000Gy (assuming 10 hours of investigation under 100Gy). And, the test was conducted under 25°C (room temperature) and 50°C respectively and the difference in impact depending on the environmental conditions was verified.

<Test system>

A constant temperature reservoir was used for simulating the temperature conditions. A thermocouple was installed inside the telescopic pipe to monitor temperature so as to ensure that there is no difference in the temperature inside the constant temperature reservoir and inside the telescopic pipe. And, a sealant that was already exposed to radiation was used for simulating the radiation dose environment.

The sealing performance was verified by subjecting the telescopic pipe to 0.1MPa of air, applying soapy water to the area around the piston part and confirming whether or not there was any leakage.

The sliding resistance was measured by pulling the piston with a load meter under every test condition.









Structure of sealed part





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6. Implementation Details

(2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc. (2) Sealing performance verification test

<Test Item>

The following 2 types of tests were conducted for the "Telescopic access equipment sealing performance verification test".

- ① Leakage check
- 2 Seal sliding resistance comparison test

<Purpose>

- 1 Leakage check
 - ⇒ To confirm whether or not the seal can prevent leakage of air under the radiation dose and temperature conditions in the investigation area.
- ② Seal sliding resistance comparison test
 - ⇒ To confirm whether or not the sliding resistance of the seal changes under the radiation dose and temperature conditions in the investigation area.

<Evaluation items, etc.>

No.	Name of the test	Evaluation item	Target (criteria)	Verification method
1	Leakage confirmation	Presence of air leakage	Air shall clearly not be leaking	Visually confirmation for formation of foam in the soapy water applied at the surface of the tip of the telescopic pipe (performed once for every condition)
2	Seal sliding resistance comparison test	Sliding resistance	Shall be equal to or less than the maximum tensile force of the cable winding equipment (Roughly) 50N or less	Measuring the sliding resistance by pulling the piston that installs the seal inside the telescopic pipe, with the load meter (performed 5 times for every condition)

<Scope of simulation of test system>

Simulation target	Simulated	Not simulated	Reason for not being simulated
	•Outer diameter / inner diameter	·Length	As it is sufficient as long as just the length required for verifying the sliding resistance is secured.
Telescopic pipe	 Otter diameter / inner diameter	 Shape of the site where the seal is installed 	As it is sufficient as long as the contact between the telescopic pipe and the seal are simulated, and the shape of the site for installing the seal does not need to be simulated (In the actual equipment, the component for pulling that is removed from the piston will be installed at the lower tip of the second stage of the telescopic mechanism)
Surrounding	•Exposure dose	·Humidity	As it is assumed that the environmental conditions are such that the characteristics of the seal cannot be changed significantly.
environment	•Temperature	• Darkness	As the environmental conditions are such that the characteristics of the seal cannot be changed.



(2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc. (2) Sealing performance verification test

Wear ring Small pneumatic packing Pneumatic cylinder packing

1 Leakage check

RID

<Test results>

- > When 0.1 MPa, which is assumed to be the maximum pressure supplied inside the telescopic pipe, was supplied, there was leakage under all conditions, and it was found that the difference in the dose and temperature conditions did not have an impact on the air sealing function.
- There was leakage from the entire circumference of the regular seal under all conditions. There was leakage from some parts of the controlled inclination type seal under all conditions, but the quantity of leakage was less in the controlled inclination type seal which has stronger adhesion.
- In order to reduce the quantity of leakage, inner surface of the telescopic mechanism needs to be improved such as by reducing its roughness (making it smoother), etc.
- The impact of leakage from each type of sealed part structures on the \geq extension/retraction movement of the telescopic access equipment was verified by conducting a telescopic access equipment behavior verification test

Result of leakage check

No.	Structure of sealed part	Exposure dose	Temperature	Result of verification
1		0Gy	25°C (room temperature)	Leakage present
2	Popular	(Unirradiated)	50°C or more	Leakage present
3	Regular	100061	25°C (room temperature)	Leakage present
4		100009	50°C or more	Leakage present
5		0Gy	25°C (room temperature)	Leakage present
6	Controlled inclination	(Unirradiated)	50°C or more	Leakage present
7	type	100061	25°C (room temperature)	Leakage present
8		1000Gy	50°C or more	Leakage present



Regular





Verification of leakage in the regular seal under 0Gy (unirradiated) and 50°C conditions



Telescopic pipe fixed on to the test rack

Verification of leakage in the controlled inclination type seal under OGy (unirradiated) and 50°C conditions





Piston (applying soapy

water to the surrounding area)

(2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc. (2) Sealing performance verification test

② Seal sliding resistance comparison test

Sliding resistance measurement results

<Test results>

- It was found that the sliding resistance tends to increase in the regular seal when it is irradiated and heated.
- The sliding resistance decreased in the controlled inclination type seal when it was irradiated, but it was found that the sliding resistance tends to increase when it is irradiated and heated, similar to the regular seal.
- As the rated tensile force of the cable winding equipment is 83N, the pipe of the regular seal can be retracted, however, it may not be possible to retract the pipe of the controlled inclination type seal.
- In order to reduce the sliding resistance, inner surface of the telescopic mechanism needs to be improved such as by reducing its roughness, etc.

Load mete	er
	Wire
Mais-Tak	
The status cl	ose at hand



Unit 2 & 3

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The test rack affixed inside the constant temperature reservoir

No.	Structure of sealed part	Exposure dose	Temperature (average) [°C]	sliding resistance under each condition [N]	average value under each condition [N]
1		0[Gy]	23	30.0 to 37.7	34.9
2	Poqular	(No irradiation)	52	35.6 to 43.7	39.1
3	Regular		23	33.0 to 42.9	38.3
4		TUUU[Gy]	51	45.8 to 54.3	51.0
5		0[Gy]	23	95.5 to 114.4	102.8
6	Controlled inclination type	(No irradiation)	51	89.8 to 119.7	104.4
7		type	23	80.4 to 95.2	85.7
8		looo[Gy]	51	104.5 to 122.0	115.0



Measurement of sliding resistance under 50°C environment

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(2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc. (3) Behavior verification test

<Test overview>

Elemental tests of the telescopic pipe with the entire 14 stage structure are planned to be conducted in FY2021. Directed towards these tests, the movement of the telescopic pipe was verified in FY2020 by partial test manufacturing a 3 stage structure, the smallest structure that can facilitate simulation of the base, middle section and the seal structure at the tip. Information contributing to designing the equipment was obtained by evaluating the behavior observed during the test.

<Test system>

The purpose of this test was to verify the extension and retraction movement of the pipe. The 3 stages at the base were simulated for the test since the entire load of the 14 stage structure was to be applied to a 3 stage structure. And, both types of seal structures - the regular (pneumatic cylinder) and the controlled inclination type were arranged for and tested respectively.



<Test items>

The following 4 types of tests were conducted for the "Telescopic access equipment behavior verification test" using a 3 stage telescopic pipe. An overview of each of these tests is provided on the following slides.

(1) Telescopic pipe extension retraction movement verification test

(2) Extension retraction movement test when the telescopic pipe is inclined

- 3 Behavior verification test when the telescopic pipe / investigation equipment get caught in the structures
- (4) Extension retraction movement verification test when foreign material adheres to the telescopic pipe



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Unit 2 & 3



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2. Feasibility study E: Performing tests, etc. (3) Behavior verification test

<Scope of simulation of test system>

Simulation target	Simulated	Not simulated	Reason for not being simulated
		Humidity, fog	As the test is under wet conditions (not simulated as an environment)
		Dose rate	CFRP strength and bonding strength has already been tested in the past. Only the sealed portion is simulated for the test.
Environmental Conditions	RPV opening size	Temperature	Only the sealed portion is simulated for the test.
		Darkness	As there is no impact on the movement behavior of the telescopic pipe
		Structures below the RPV bottom opening part	The movement behavior of the telescopic pipe is verified in this test. Movement when the structures are simulated is planned to be verified during the mock-up test implemented prior to the on-site investigation.
		Camera not mounted	As the presence/absence of the camera image does not impact the extension retraction movement.
Investigation equipment	 Mass Tapering shape 	Shapes other than the tapering shape	As the shape of the investigation equipment does not impact the extension retraction movement.
		Mechanism (No tilting movement, no extension of illumination	As the impact of change in the center of gravity of the investigation equipment when the mechanism is moved, on the extension retraction movement will be verified when the 14 stage telescopic pipe is test manufactured.
Telescopic pipe	 Shape (3 stage, tapering) Mass (equivalent to that of 14 stages (simulated with partial weight)) Mechanism (seal, etc.) 	Entire length (14 stages)	The movement and behavior of the telescopic pipe is verified in this test. The length-wise impact of the inclination, vibrations and deflection when the telescopic mechanism is gradually extended, will be verified when the 14 stage telescopic pipe is test manufactured next year.
Cable winding equipment	 Winding mechanism Pressure resistant case Torque measurement function 	Flexural rigidity of the investigation equipment cable	As it is believed that the flexural rigidity of the cable does not impact the extension retraction movement and since it will be verified when the 14 stage telescopic pipe is test manufactured next year.
	Thickness of the investigation equipment cable	Tensile strength of the investigation equipment cable	As the required tensile force for the investigation equipment cable is verified in this test
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(2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc. (3) Behavior verification test

<Test apparatus>









3 stage telescopic pipe (when completed) 3 stage telescopic pipe (when completed) extended)

Pressure verifying vibrations Operation panel operation panel



Console

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convergence time and

verified based on the

image from the bird's

vibration cycle

eye view camera

vibrations.

If the telescopic pipe vibrates,

performed after the vibrations

extension/retraction

stop

Convergence time and

vibration cycle

of

are

	, etc.	(S) Denavio	or vernication test	•			
(1) Telescopic pipe extension retraction movem	ient ve	erification test					
<purpose></purpose>	<evalu< td=""><td colspan="6"><evaluation etc.="" items,=""> (~1) Numerical values obtained when the test is performed using a 3 stage telesco</evaluation></td></evalu<>	<evaluation etc.="" items,=""> (~1) Numerical values obtained when the test is performed using a 3 stage telesco</evaluation>					
vertical direction is possible when the 3 stage telescopic pipe	No.	Evaluation item	Target (criteria)	Policy for setting target values	Verification method		
and cable winding equipment are combined and a heavy object weighing as much as the investigation equipment is mounted at the tip of the telescopic pipe, and to verify the movement characteristics under those circumstances. <conceptual diagram="" of="" test="" the=""> Extent of deviation at the tip</conceptual>		Extension height	Equivalent to 3 stages	Maximum extension of the telescopic pipe that is test manufactured	Measurement using a laser range finder		
		Air pressure required while extending	0.1MPa or less	Maximum design pressure or less	Measurement of pressure of air injected at each stage, using a pressure gauge		
Vibration in the horizontal direction at the tip	①-3	Cable tensile force required while retracting	50N or less	Equal to or less than the maximum tensile force of the cable winding equipment	Evaluated based on the cable winding equipment drum driven motor torque		
(evaluation item (1)-6)	①-4	Accuracy of the measurement of extension/retracti on using the winding equipment	Error ±30mm or less	The maximum error so that at least 1/4 of the images overlap, when the camera moves in the vertical direction so that 1/3 of the images overlap, while generating images through the cylinder.	At every 0.5m the value obtained from the measurement by means of the winding equipment and the actual value measured by the laser range finder are compared.		
Cable tensile force required while retracting (evaluation item ①-3) Accuracy of the measurement of /extension/retraction using	①-5	Extent of deviation at the tip (backlash)	Approx. 16mm or less (*1) (at full length: 65mm or less)	The permissible deviation when 3 stages are extended is set such that the 9th stage of the telescopic pipe (ϕ 57mm) does not come in contact with the reactor bottom opening (ϕ 187mm).	Horizontal load sufficient to eliminate the backlash is applied to the tip at each stage of the telescopic pipe to verify the displacement by means of the plumb bob.		
/ the winding equipment					The presence of		

<Purpos

6. Implementation Details

(2) Development of the bottom access investigation method

2 Feasibility study F: Performing tests etc. (3) Rehavior verification test

a 3 stage telescopic pipe are listed.

is measured). Measurement is conducted 3 times.

Other items to be

verified

Method of coordinated

control of air pressure reduction and tensile

telescopic mechanism

-Whether or not there

is irregular winding by

the winding equipment

•Whether or not the

limit of extending the

telescopic pipe can be

determined based on

the cable tensile force

determined, a soft limit

is applied based on the

valued obtained when

the extension/retraction

(if it cannot be

force required for

winding when the

is being retracted

RD

Extension height

(evaluation item 1)-1)

the winding equipment (evaluation item 1-4) Vibration in the 1)-6 horizontal Air pressure required direction at the tip while extending (evaluation item 1)-2)



(2) Development of the bottom access investigation method

- 2. Feasibility study E: Performing tests, etc. (3) Behavior verification test
- ① Telescopic pipe extension retraction movement verification test <Results using the regular seal>
- It was confirmed that extension retraction movement is possible with the tensile force of the cable winding equipment and under maximum design pressure or less.
- There were no vibrations during the extension and the retraction and the extent of deviation due to backlash was within the permissible range.
- The error in the accuracy of the measurement of extension/retraction increased as the telescopic pipe extended, but this issue is expected to be resolved by controlling the extension with the help of the reinforced cable being planned.
- The tensile force was 220N at maximum (momentary force / can be reproduced when the retraction of second pipe starts) as against the targeted 50N, but the pipe was retracted. The force during retraction was about 50N to 130N.

<Results using the controlled inclination type seal>

- The sliding resistance was unexpectedly high, the motor torque was insufficient, and the pipe was not retracted. Hence extension was verified only once.
- The extent of deviation at the tip was half of that using the regular seal and it was found that a wear ring is useful.

<Test picture>

Plumb bob string



backlash



Telescopic pipe during extension

No.	Evaluation item	Target (criteria)		Result	
1	Extension beight	Envirolant to 2 stance	Regular	1 st time to 3 rd time: equivalent to 3 stages (maximum 2300mm)	0
	Extension height		Controlled inclination type	1 st time: equivalent to 3 stages (maximum 2300mm)	0
	Air pressure		Regular	1 st time to 3 rd time: 0.04MPa	0
0-2	extending	0.1MPa or less	Controlled inclination type	1 st time: 0.05MPa	0
(1)-3	Cable tensile force required while retracting (determined based on the value from	sile force /hile ed based 50N or less ue from		1 st time: Maximum 120N 2 nd time: Maximum 220N 3 rd time: Maximum 220N	△ (The pipe can be retracted, but the tensile force while retracting may exceed the rated value of 83N.)
	the motor torque monitor)		Controlled inclination type	—	×
<u>(</u>]-4	Accuracy of the measurement of extension/retraction using the winding equipment	Error ±30mm or less	Regular	1 st time: 29mm 2 nd time: 22mm 3 rd time: 20mm	0
			Controlled inclination type	1 st time: 23mm (error only during extension)	0
①-5	Extent of deviation at the tip	xtent of deviation 16mm or less t the tip (at full length: 65mm or packlash) less)	Regular	1 st time: 5.5mm 2 nd time: 7mm 3 rd time: 6mm	0
	(backlash)		Controlled inclination type	1 st time: 3.5mm	0
①-6	Vibration in the horizontal direction at the tip	n the Convergence time and direction vibration cycle	Regular	No vibrations (There are no vibrations even if it is bent by deliberately applying load)	0
			Controlled inclination type	No vibrations (behavior only while extending)	0



<List of results>





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(2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc. (3) Behavior verification test



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- (2) Development of the bottom access investigation method
- 2. Feasibility study E: Performing tests, etc. (3) Behavior verification test
- ① Telescopic pipe extension retraction movement verification test

<Summary of the extension retraction movement verification test>

- The test was conducted 3 times for the telescopic pipe with the regular seal and it was confirmed that the required air pressure, cable tensile force and extension/retraction measurement accuracy can be reproduced.
- While retracting the telescopic pipe, with the regular seal, the pipe needed to be retracted while exceeding the rated tensile force. In order to be able to retract the telescopic pipe with a tensile force that is equal to or lower than the rated tensile force, measures need to be taken to reduce the sliding resistance between the inner surface of the telescopic pipe and the packing.
- While extending the telescopic pipe, with the regular seal, it was found that the gap between the set pressure of the electropneumatic regulator installed on the air supply line and the supplied pressure tends to increase with the extension of the telescopic pipe. Meanwhile, with the controlled inclination type seal, there is no gap between the set pressure and the supplied pressure even when the telescopic pipe is extended. It is presumed that this is because of the difference in the amount of leakage from the compressed gas packing supplied inside the telescopic pipe.
- The plan was to determine that extension has been completed when the tensile force becomes zero, but it was found that the tensile force does not become zero simultaneously with the completion of extension. Detection of completion of extension of the telescopic pipe needs to be studied including cases when the telescopic pipe does not have to be extended to the maximum.
- It was found that even if the tensile force exceeds the upper limit when the telescopic pipe is retracted, by resuming retraction after the pressure inside the telescopic pipe (supplied pressure) decreases, retraction can be continued by reducing the required tensile force. (At the time of retracting the telescopic pipe, the pressure inside the telescopic pipe goes on increasing during retraction, but when retraction is stopped, the pressure decreases due to the electropneumatic regulator (air pressure regulating valve).)



- (2) Development of the bottom access investigation method
- 2. Feasibility study E: Performing tests, etc. (3) Behavior verification test
- ② Extension retraction movement verification when the telescopic pipe is inclined

<Purpose>

To ascertain the maximum inclination at which the telescopic pipe can be extended/retracted, with the same configuration as "① Telescopic pipe extension retraction movement verification test"

<Conceptual image of the test>

<Evaluation items, etc.>

n inclination at	No.	Evaluation item	Target (criteria)	Policy for setting target values	Verification method	Other items to be verified
an be same opic pipe extension ation test" est>	② −1	Inclination at which the pipe can be extended/retracted up to 3 stages	Can be extended/retracted	As the telescopic pipe has been designed on the premise of being able to extend and retract vertically based on the investigation conditions, the inclination at which the pipe can be extended/retracted shall be verified without setting the target value (maximum 5°)	The inclination of the installation stand of the telescopic pipe is verified by means of an angle meter.	
	Q-2	Air pressure required while extending	0.1MPa or less	Maximum design pressure or less	Measurement of pressure of air injected at each stage, using a pressure gauge	Whether or not there is irregular winding by the winding equipment Detecting when the telescopic pipe has
Tensile force required while retracting (evaluation item 2 -3) Accuracy of the measurement of	2-3	Tensile force required while retracting	50N or less	Shall be equal to or less than the maximum tensile force of the cable winding equipment	Evaluated based on the cable winding equipment drum driven motor torque	been extended to its full length: depends on the accuracy of the measurement of extension/retraction
Air pressure required while extending (evaluation item 2 -4)	@-4	Accuracy of the measurement of extension/retraction using the winding equipment	Error ±30mm or less	The maximum error so that at least 1/4 of the images overlap, when the camera moves in the vertical direction so that 1/3 of the images overlap, while generating images through the cylinder.	Value obtained from the measurement by means of the winding equipment and the actual value measured by the laser range finder are compared.	



Inclination at which the pipe can be extended

up to 3 stages (evaluation item 2 -1



(2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc. (3) Behavior verification test

2 Extension retraction movement verification when the telescopic pipe is inclined

<Results using the regular seal>

It was found that the pipe can be extended even with an inclination of 5° (upper limit of test). It is conceivable that the lower end of the pipe would get caught due to the moment resulting from self weight, and that the tensile force required for retraction increases as compared to vertical movement, but it was found that the pipe can be retracted at an inclination of 3°. This is expected to be resolved by changing the seal structure and controlling the backlash. Additionally, the allowable angle of inclination is expected to increase by further reducing the sliding resistance of the seal.

<Results using the controlled inclination type seal>

When the vertical extension retraction movement was verified, the sliding resistance was unexpectedly high, the motor torque was insufficient, and the pipe was not retracted. Hence this test was not performed.

<Pictures of testing>

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Extension of a telescopic pipe at an inclination of 5°

<List of results> Conducted only once for each condition (regular)

No.	Evaluation item	Target (criteria)		Result	
@-1	Inclination at which the pipe can be extended/retract ed up to 3	Can be extended/retracted	Regular	Inclination 3°: Can be extended/retracted Inclination 4°: Can be extended only Inclination 5°: Can be extended only	O (Precondition for operating the telescopic pipe vertically)
	stages		Controlled inclination type	-	_
⊘ −2	Air pressure required while extending	0.1MPa or less	Regular	Inclination 3°: 0.04MPa Inclination 4°: 0.04MPa Inclination 5°: 0.04MPa	0
			Controlled inclination type	_	—
Q-3	Tensile force required while retracting	50N or less	Regular	Inclination 3°: Maximum 270N Inclination 4°: Cannot be retracted Inclination 5°: Cannot be retracted	\triangle (The pipe can be retracted, but the tensile force while retracting may exceed the rated value of 83N.)
			Controlled inclination type	-	_
@-4	Accuracy of the measurement of extension/retract ion using the winding equipment	Error ±30mm or less	Regular	Inclination 3°: 26mm Inclination 4°: Not evaluated (*1) Inclination 5°: 15mm	0
			Controlled inclination type	-	—

(*1) Not evaluated as the characteristics can be ascertained by evaluating the upper limit / lower limit under test conditions.



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- (2) Development of the bottom access investigation method
- 2. Feasibility study E: Performing tests, etc. (3) Behavior verification test

2 Extension retraction movement verification when the telescopic pipe is inclined (regular seal, angle of inclination 3°)



While extending the pressure supplied is 30kPa ~ 40kPa While retracting the pressure supplied is 5kPa

(2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc. (3) Behavior verification test

③ Behavior verification test when the telescopic pipe / investigation equipment get caught in the structures

<Purpose>

To verify that with the same configuration as "① Telescopic pipe extension retraction movement verification test" when the telescopic pipe gets caught in the structures while being extended, the catch can be eliminated by following the precedent of the taper installed on the telescopic pipe or the investigation equipment.

<Conceptual diagram of the test>

Simulated RPV opening part (Using Unit 2 as reference, where the conditions for the size of the opening are stringent, there is an opening of φ 187mm at



Required tensile force for the investigation equipment cable while eliminating the catch (evaluation item ③ -3)

Propriety of eliminating the

catch while being retracted

equipment taper (evaluation item (3) -2)

pipe taper

by means of the investigation

Propriety of eliminating the catch while being extended by means of the telescopic

(evaluation item (3) -1)

<Evaluation items, etc.>

No.	Evaluation item	Target (criteria)	Policy for setting target values	Verification method	Other items to be verified
3—1	Propriety of eliminating the catch while being extended by means of the telescopic pipe taper	Elimination	Verifying that there is no problem with the designed taper angle	Visual confirmation	
③−2	Propriety of eliminating the catch while being retracted by means of the investigation equipment taper	Elimination	Verifying that there is no problem with the designed taper angle	Visual confirmation	•Whether or not the pip will get caught at other locations where the taper has not been provided
3-3	Required tensile force for the investigation equipment cable while eliminating the catch	50N or less	Shall be equal to or less than the maximum tensile force of the cable winding equipment	Evaluated based on the cable winding equipment drum driven motor torque	



(2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc. (3) Behavior verification test

3 Behavior verification test when the telescopic pipe / investigation equipment get caught in the structures

3.

3.

3.

<Results using the regular seal structure>

- The location where the opening rubs against the pipe (interference of telescopic pipe taper of 8.5mm and investigation equipment taper of 11mm) and the location that reduces the interference between the taper and the opening (interference of telescopic pipe taper of 3mm and investigation equipment taper of 7mm), were evaluated for the location for the opening.
- Since the telescopic pipe has little backlash and deflection, the pipe cannot be extended/retracted if it was placed such that it rubs against the opening. When the interference was reduced, although it was extended, it was not retracted.
- Since the 14 stage telescopic pipe becomes guite long and thus becomes less rigid, evaluation will be performed during the 14 stage telescopic pipe test as well. And, as the arm-type access equipment for retrieval is likely to pass through due to its deflection during actual operation, the rigidity characteristics of the access equipment will be verified in future and the demonstration method will be studied.

<Results using the controlled inclination type seal structure>

When the vertical extension retraction movement was verified, the sliding resistance was unexpectedly high, the motor torgue was insufficient, and the pipe was not retracted. Hence this test was not performed.

<Test picture> Simulated opening

RID





Simulated opening created

No.	Evaluation item	Target (criteria)	Result					
3—1	Propriety of eliminating the catch while being extended by means of the telescopic pipe taper	Elimination	Regular	Interference 8.5mm: Cannot be extended Interference 3mm: Can be extended (required pressure 0.04MPa)	x (The arm type access equipment is likely to pass through due to its deflection.)			
			Controlled inclination type	-	—			
3–2	Propriety of eliminating the catch while being retracted by means of the investigation equipment taper	Elimination	Regular	Interference 11mm: Cannot be retracted Interference 7mm: Cannot be retracted	x (The arm type access equipment is likely to pass through due to its deflection.)			
			Controlled inclination type	—	_			
3-3	Required tensile force for the investigation equipment cable while eliminating	50N or less	Regular	(The catch was not eliminated under any of the conditions)	x (Motor torque needs to be increased)			
	the catch		Controlled inclination type	_	_			
10	and the second distance of the second distanc							

<List of results>Conducted only once for each condition (regular)



Location where the opening rubs against the pipe

Location where the interference is reduced

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(2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc. (3) Behavior verification test

(4) Extension retraction movement verification test when foreign material adheres to the telescopic pipe

No.

(4)-1

(4)-2

<Purpose>

To verify whether or not the telescopic pipe can be retracted when its outer surface is wet or when foreign material is adhered to it, with the same configuration as "
 Telescopic pipe extension retraction movement verification test".

The following 2 types of particle sizes were selected as particles that enter the gap (200µm) between the pipes.

(b) Particle size 100µm (alumina)

<Conceptual diagram of the test>

camera moves in the **(4)-3** measurement of Error ±30mm or less vertical direction so that extension/retraction 1/3 of the images overlap, Moistening the while generating images surface, making through the cylinder. foreign material adhere to the surface Upper stage telescopic pipe Tensile force required Scraper while retracting (evaluation item $(\overline{4})$ -1) Dust seal Upper stage pipe Stopper ring Top ring Lower stage telescopic pipe Collar Accuracy of the Lower stage pipe measurement of Pneumatic cylinder type packing extension/retraction (evaluation item (4)-3) Piston Air pressure required while extending Gap 0.2mm (evaluation item (4)-2)

(a) Particle size 15µm (soil)



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Verification method

Evaluated based on the

equipment drum driven

pressure of air injected

at each stage, using a

At every 0.5m the value

cable winding

motor torque

Measurement of

pressure gauge

obtained from the

measurement by

means of the winding

actual value measured

equipment and the

by the laser range

finder are compared.

Other items to be

verified

Whether or not there is

irregular winding by the

winding equipment

Policy for setting target

values

Shall be equal to or less

than the maximum tensile

force of the cable winding

Maximum design pressure

The maximum error so

that at least 1/4 of the images overlap, when the

equipment

or less

<Evaluation items, etc.>

Tensile force

required while

Air pressure

required while

Accuracy of the

retracting

extendina

Evaluation item

Target (criteria)

50N or less

0.1MPa or less

(2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc. (3) Behavior verification test

④ Extension retraction movement verification test when foreign material adheres to the telescopic pipe

<Results using the regular seal>

- Particles of (a) size 15µm (soil) and (b) size 100µm (alumina) were made to adhere to the 2nd stage pipe and the pipe was extended and retracted. (150Mm gap between the pipes)
- There was no change in behavior even when the pipe was extended and retracted while powder a and powder b adhered to it. The tensile force while retracting was also in the range of roughly 50N to 130N and thus it was found that there was no difference compared to when no powder adhered to the pipe surface.
- When the telescopic pipe was disassembled and checked, it was found that the powder had not entered the seal part or inside the pipe and thus it was confirmed that the dust seal was effective.

<Results using the controlled inclination type seal>

- When the vertical extension retraction movement was verified, the sliding resistance was unexpectedly high, the motor torque was insufficient, and the pipe was not retracted. Hence this test was not performed.
- <Test picture>





Inside the 1st stage of the pipe after the test

No. Evaluation item Target (criteria) Result Δ (The pipe can be Powder a: Maximum 230N retracted, but the Powder b: Maximum 130N Regular Tensile force required tensile force may **(4)-1** 50N or less Retraction possible in either case exceed the rated while retracting value of 83N.) Controlled inclination type Powder a: 0.04MPa Powder b: 0.04MPa Regular 0 (Can be extended just like when Air pressure required **(4)-2** 0.1MPa or less no foreign material is adhered) while extending Controlled inclination type Powder a: 22mm 0 Accuracy of the Regular Powder b: 14mm **(4)-3** Error ±30mm or less measurement of Controlled extension/retraction inclination type

Powder deposited on to the outer peripheral surface of the pipe at the 2nd stage Power (b) has a larger particle size and hence the surface is moistened and then powder is deposited.

<List of results> Conducted only once for each powder (regular)



- (2) Development of the bottom access investigation method
- 2. Feasibility study E: Performing tests, etc. (3) Behavior verification test

(4) Extension retraction movement verification test when foreign material adheres to the telescopic pipe (regular seal, soil)



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- (2) Development of the bottom access investigation method
- 2. Feasibility study E: Performing tests, etc. (3) Behavior verification test

④ Extension retraction movement verification test when foreign material adheres to the telescopic pipe (regular seal, alumina)







(2) Development of the bottom access investigation method

2. Feasibility study E: Performing tests, etc. (3) Behavior verification test

Summary (regular seal)

- It was verified that the telescopic pipe can be extended/retracted with the configuration of the telescopic pipe and cable winding equipment being considered (Leakage did not have any impact). However, as the maximum required tensile force when the telescopic pipe is vertical was 230N as against the tensile force of 83N resulting from the rated torque of the motor of the cable winding equipment, it became evident that the sliding resistance of the seal of the telescopic pipe needs to be reduced.
- As it was confirmed that the telescopic pipe can be extended/retracted at an inclination of 3°, the error in installation by means of the arm type access equipment for retrieval will be verified in future and measures will need to be studied as necessary.
- Even if foreign material (powder) adhered to the telescopic pipe, the powder did not get stuck inside the pipe and there was no major difference in the required tensile force. Thus the effectiveness of the dust seal was verified.

Summary (controlled inclination type seal)

> The sliding resistance was unexpectedly high, the motor torque was insufficient, and the pipe was not retracted. Hence it was only verified whether or not the pipe was extended.



Unit 2 & 3

No. 96

6. Implementation Details No. 97 Unit 2 & 3 (2) Development of the bottom access investigation method 2. Feasibility study E: Performing tests, etc. Feasibility of the 14 stage telescopic pipe No. Items **Evaluation** Reason It was verified that a 3 stage telescopic pipe can be extended with a pressure of 0.04MPa or less when there is regular packing. However, as the telescopic pipe is extended and gets longer, the gap between the supplied pressure and the adjusted pressure Extension increases. When the 14 stage telescopic pipe continues to be extended, the supplied pressure may not rise even if the set 1 Acceptable pressure is increased. This increase in gap is not seen in case of the controlled inclination type seal structure in which there is less movement leakage as compared to the regular seal. Hence it is believed that the leakage from the packing is the cause. \Rightarrow Issue (1): Reducing the amount of leakage A 3 stage telescopic pipe was retracted when there was regular packing. However, it was found that the tensile force while Retraction retracting exceeds the rated tensile force of the motor. The sliding resistance needs to be reduced in order to reduce the required 2 Acceptable movement tensile force. \Rightarrow Issue 2: Reducing the sliding resistance When the 3 stage telescopic pipe was completely extended and horizontal load was applied, there was misalignment resulting from the backlash of 3mm in case of the controlled inclination type seal structure and a backlash of 7mm in case of the regular Ability to seal. The pipe that passes through the ϕ 187mm opening assumed to be present at the RPV bottom is the 9th stage (ϕ 57mm). The pass through misalignment due to the backlash when the pipe is extended up to the 9th stage (length 6.9m) is 21mm in case of the regular seal 3 Good φ187mm and 10mm in case of the controlled inclination type seal. Hence it was verified that telescopic pipe backlash does not affect passing through the ϕ 187mm opening in the case of the regular seal, with which the 3 stage telescopic pipe was opening extended/retracted. Further, the misalignment caused by the backlash when the 14 stage telescopic pipe is extended (length 10.4m) is 31mm in the case of the regular seal and 10mm in the case of the controlled inclination type seal. The catch was not eliminated even with a regular packing in a 3 stage telescopic pipe. The sliding resistance of the packing Catch structure needs to be reduced in order to make it easier to eliminate the catch during retraction. Further, when using the actual elimination Acceptable 4 equipment, since the arm type access equipment bends, it is expected to become easier to eliminate the catch as well. \Rightarrow Issue 2 performance : Reducing the sliding resistance

Issues such as high sliding resistance or leakage from the sealed portion came forth, however, it was evaluated that the mechanism itself was feasible.

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(2) Development of the bottom access investigation method

2. Feasibility study F: Evaluation based on the test results, etc.

O Changing the folds on the inner surface of the CFRP so that they are in a single direction

The inner surface of the current pipe is not smooth as it is made of a plain carbon fiber weave. Hence the tensile force required while retracting the telescopic pipe and the amount of leakage from the packing contact area need to be reduced by smoothening. Therefore, changing the orientation of the folds so that they face a single direction in order to smoothen the inner surface of the pipe that comes in contact with the packing, will be studied.

O Changing the seal structure

A structure combining the pneumatic cylinder packing (GLY) of the regular seal in which there is less sliding resistance and the wear ring in which there is less misalignment of the tip, will be studied.

• In addition to the above-mentioned issues, increasing the torque (cable winding force) as much as possible while considering dimensional constraints of the cable winding equipment will be included in the design study as well.

• As an alternative plan in case issues ① and ② cannot be resolved, the use of aluminum pipes that have a proven track record and have a less rough surface will be considered, and basic data will be obtained through a seal function verification test. However, using aluminum material has its demerits from the viewpoint of strength, and, the equipment becomes heavier as well. These will need to be considered if aluminum is to be used.



The effect of sealing performance will be verified by means of a verification test considering measures for reducing the amount of leakage and the sliding resistance, and the feasibility of the method is planned to be verified through elemental tests using a 14 stage telescopic pipe.



[•] The following proposals are being studied in response to issues ①: Reducing the amount of leakage and its issue ②: Reducing the sliding resistance.



6. Implementation Details (2) Development of the bottom access investigation

(2) Development of the bottom access investigation method

2. Feasibility study F: Evaluation based on the test results, etc. <Investigation plan>

The plan is to perform the investigation using the telescopic access equipment following the steps mentioned below. The plan is scheduled to be executed in FY2021.

Conceptual image of bottom access investigation in Unit 2

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Unit 2 & 3

No. 99

No. 100

7. Summary

(1) Advancement of machining technology for the top access investigation method

- Alternative machining technologies were investigated and evaluated, and machining technology in which hole saw cutting, circular saw cutting and laser cutting are added to the AWJ cutting technology was selected as machining technology that reduces the generation of secondary waste.
- •Reducing the size of the nozzle used in AWJ, optimizing machining parameters such as the jet spray angle, the cutting location, etc., were studied. In addition, equipment and tools required if hole saw cutting, circular saw cutting and laser cutting were to be used, were studied as well.
- Simple tests for verifying the cutting performance of the machining technologies were conducted and it was determined that there are prospects of AWJ cutting and laser cutting being applied (Refer to the table on the right for the combinations of cutting direction and method).



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7. Summary (2) Development of the bottom access investigation method

- In Unit 1, since the size of opening at the RPV bottom is assumed to be large, it was decided to develop a method of accessing the inside of the RPV by means of a drone (wired/wireless) by using the crawler type access equipment being developed as part of the Detailed Investigation inside PCV PJ. Simple flight tests were performed for evaluating the feasibility of accessing inside RPV by means of a drone. A wired drone consisting of a drone and a cable drum and a wireless drone consisting of a drone and extension rod were selected.
- In Unit 2 and 3, since the size of the opening at the RPV bottom is assumed to be small, it was decided to develop a method
 of accessing inside RPV by mounting a telescopic pipe on the arm type access equipment for fuel debris retrieval, the scale
 of which was gradually increased. Simple tests were performed for evaluating the feasibility of the telescopic access
 equipment.



Unit 1: Conceptual image of access using a drone



Unit 2 & 3: Conceptual image of access using a telescopic pipe



No. 101

7. Summary

Remaining issues and plan for FY2021

(1) Advancement of machining technology for the top access investigation method

Application of the machining technologies (AWJ/Laser) narrowed down based on the results of simple tests, besides the steam separator, are planned to be studied, issues in applying the technologies to actual equipment and further improvement items are planned to be identified and related measures are planned to be implemented.

(2) Development of the bottom access investigation method

• Based on the results of simple tests, conceptual designing and elemental tests on drones (wired/wireless) for Unit 1 are planned to be conducted in FY2021.

• According to the results of simple tests the telescopic access equipment for Unit 2 & 3 can be extended, however, the sliding resistance is unexpectedly high and hence further improvement is needed. Conceptual designing considering measures for reducing sliding resistance and amount of leakage will be undertaken and elemental tests using a 14 stage telescopic pipe are planned to be implemented in FY2021.

Additionally, information on the connection with the arm type access equipment for fuel debris retrieval, design information, etc. is planned to be verified and reflected.